

# Simulation of Electric Machines and Drives using the **Machines** and the **SmartElectricDrives** **Libraries** **Part II**

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- Chapter 2: The SmartElectricDrives Library - Introduction
- Chapter 3: DC Circuits
- Chapter 4: DC Machines
- Exercise 1: Examples with a Chopper and a DC Machine

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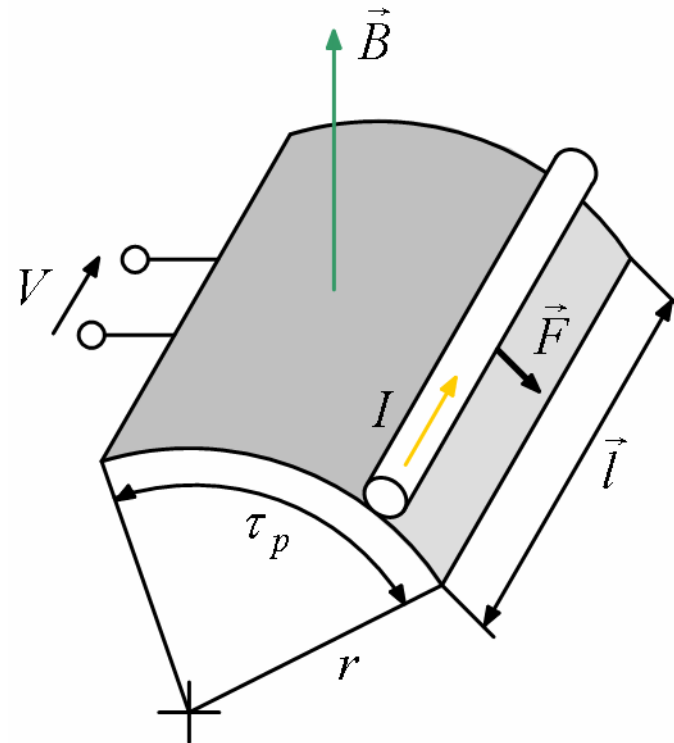
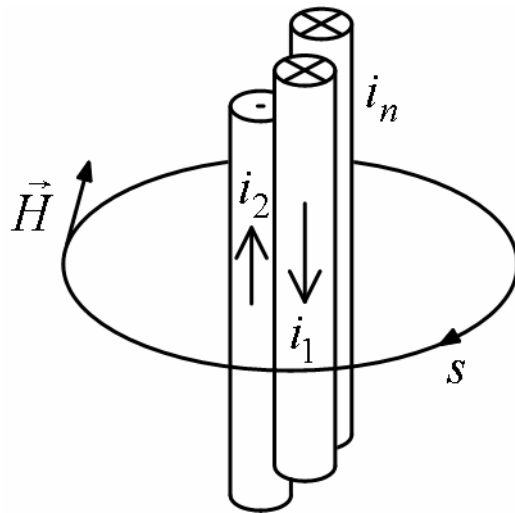
- Chapter 5: Single Phase AC Circuits
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Synchronous Induction Machines (PMSM)
- Chapter 10: DCAC Converters
- Exercise 2: Examples with a Permanent Magnet  
Synchronous Induction Machine

# Contents

- Chapter 11: Asynchronous Induction Machines
- Exercise 3: Examples with an Asynchronous Induction Machine
- Exercise 4: Automotive Applications

# Basics and Terms of Electrical Engineering

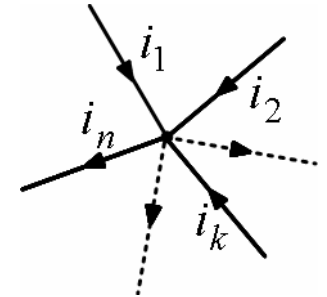
## Chapter 1



# Kirchhoff's Laws

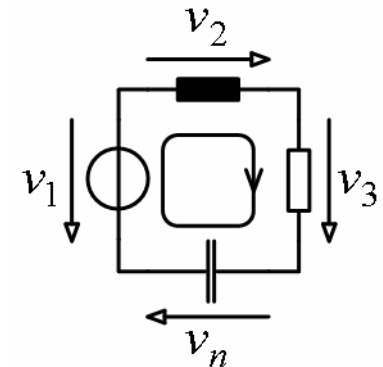
- The algebraic sum of all currents entering and exiting a node equals zero.

$$\sum_{k=1}^n I_k = 0 \quad n = \text{number of currents}$$



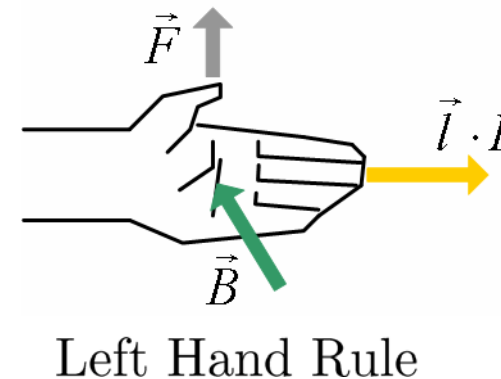
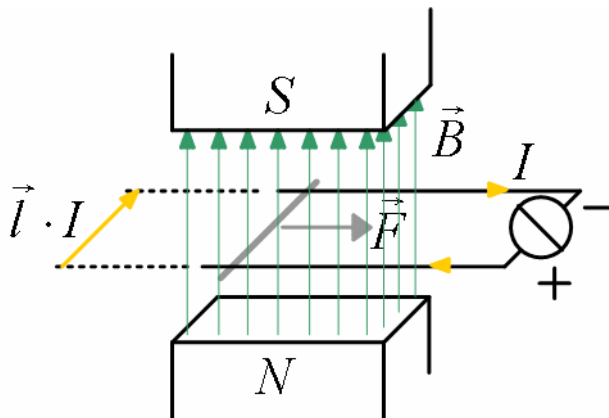
- The algebraic sum of all voltages in a loop equals zero.

$$\sum_{k=1}^n V_k = 0 \quad n = \text{number of voltages}$$



# Lorentz Force

- Force on a current carrying wire in a magnetic field



$$\vec{F} = I (\vec{l} \times \vec{B})$$

# Principle of Electric Machines

- Flux linkage

- $\Psi = B \cdot \tau_p \cdot l$

- Speed

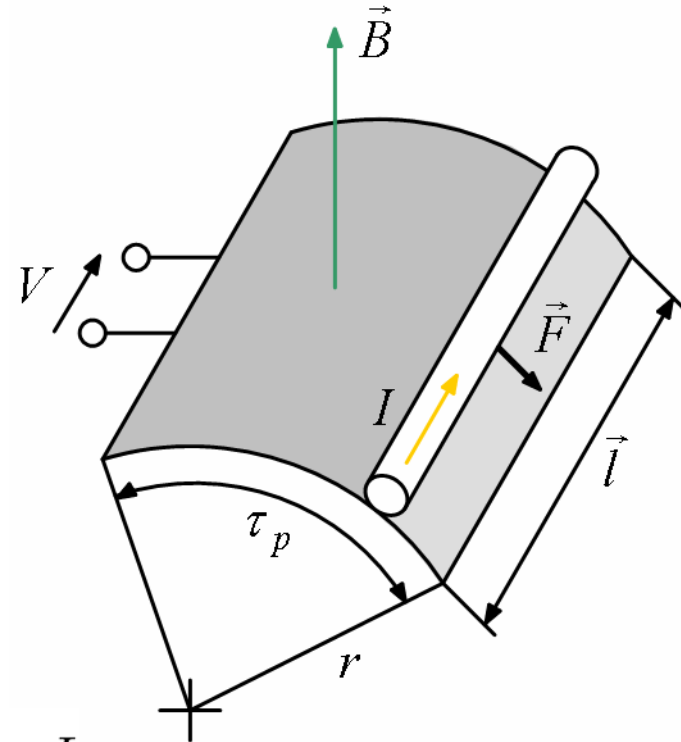
- $v = r \cdot \Omega_m$

- Induced Voltage

- $V = B \cdot l \cdot v = \frac{r}{\tau_p} \cdot \Psi \cdot \Omega_m$

- Torque

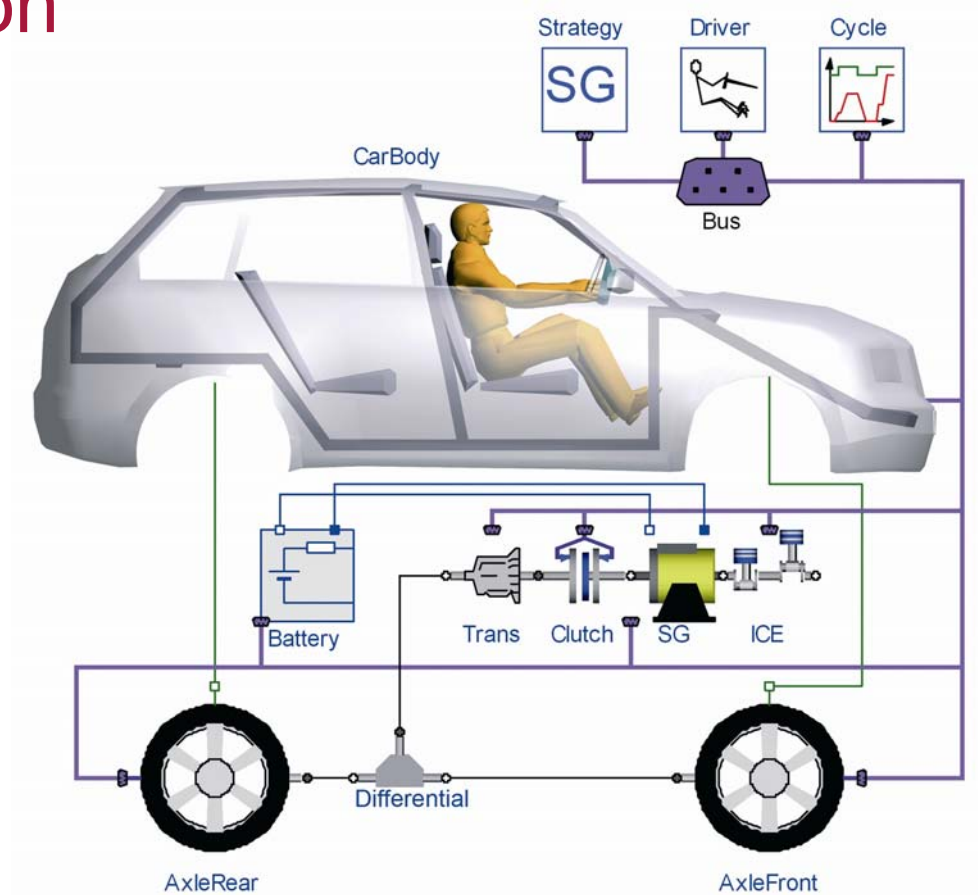
- $T = \left| \vec{F} \times \vec{r} \right| = I \cdot B \cdot l \cdot r = \frac{r}{\tau_p} \cdot \Psi \cdot I$





# The SmartElectricDrives Library - Introduction

## Chapter 2



# Overview

- Major components of the SED library
  - Asynchronous induction machines, permanent magnet synchronous induction machines, dc machines
  - Field oriented control, brushless dc control
  - Converters (ideal, switching), sources (batteries, supercaps, fuel cells)
- Application examples
  - Hybrid electric vehicles (HEVs), electric vehicles (EVs)
  - Starter / generator, electrically operated auxiliaries
  - Machine-tools and robotics
  - Paper mills, mining
  - Construction machinery, assembly lines
  - etc.

# Application Specific Drive Design I

## Practical Considerations

- Various technologies (e.g. batteries, supercaps, fuel cells etc.)
- Matching the right components based on their specifications
- Maximizing the efficiency of the entire drive system
- Comprehensive analysis of dynamic effects
- Component security (Currents, Voltages, etc.)
- Controller calibration (Dynamic characteristics and static characteristics)

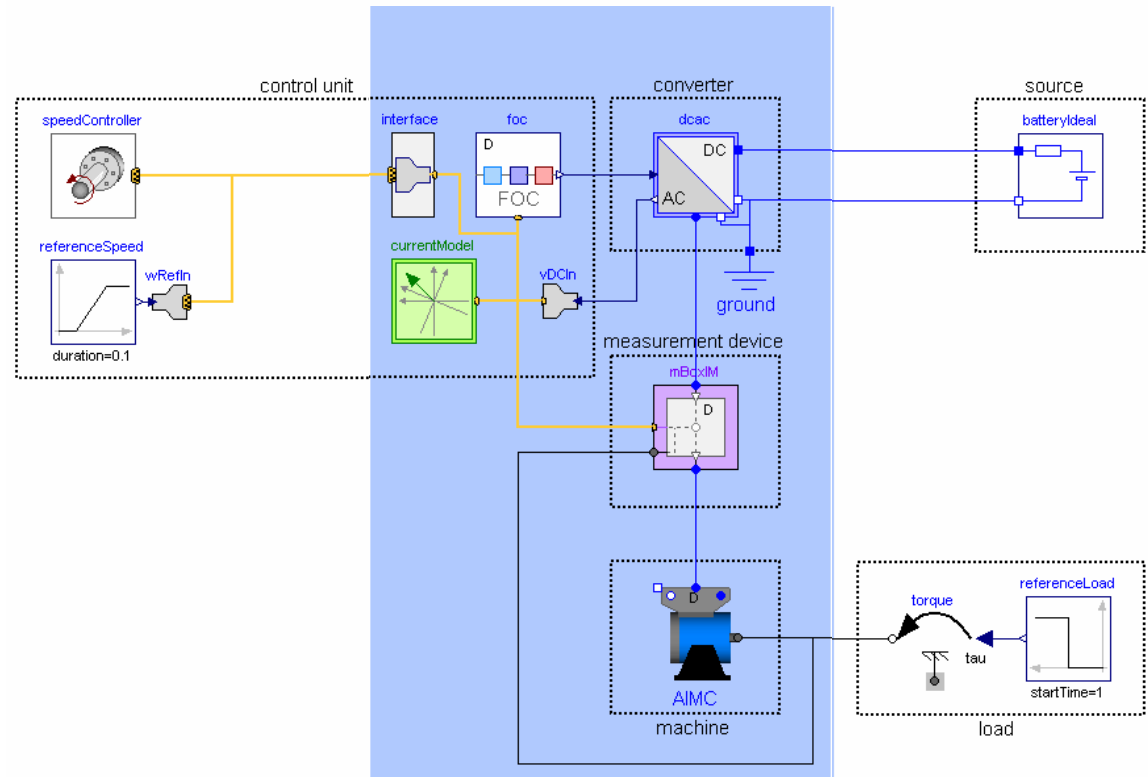
# Application Specific Drive Design II

## Software Requirements

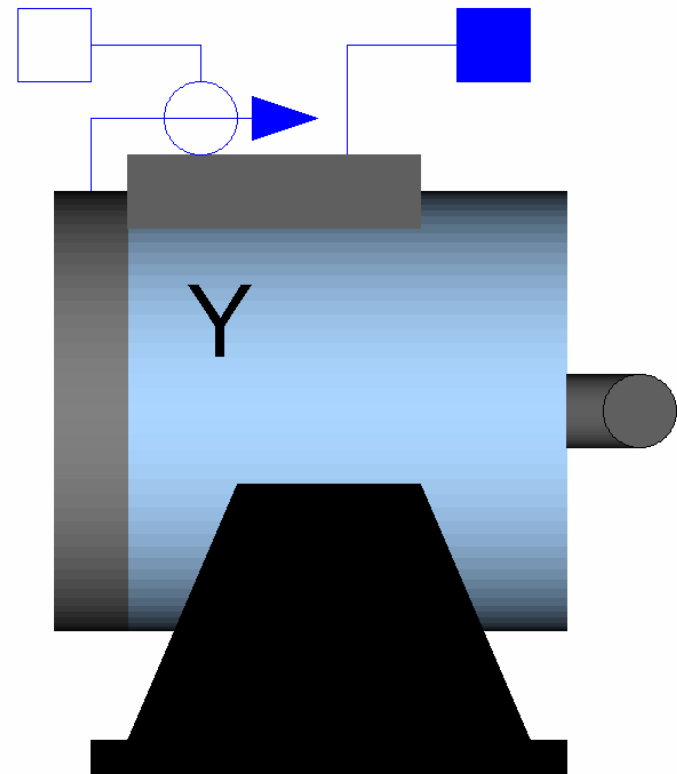
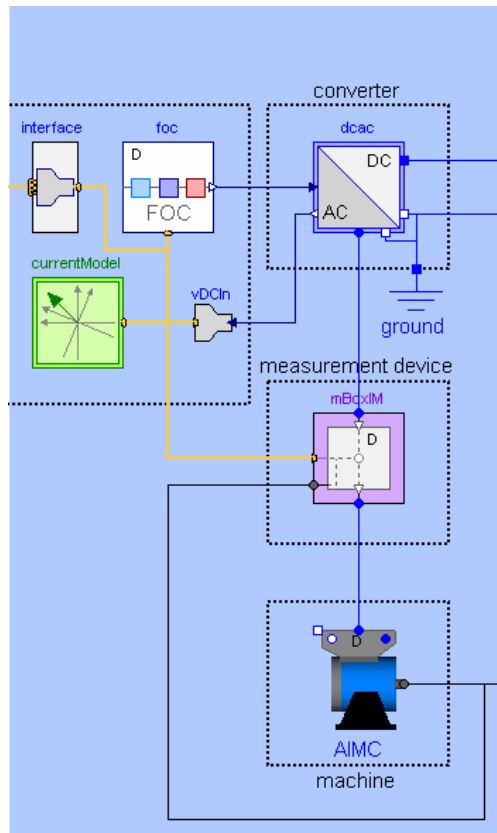
- Hybrid systems
  - Simulation of mechanical and electrical components at the same time
  - User friendliness
- High processing effort
  - Definition of different layers of abstraction
- Short development cycles
  - Automation of development procedures with 'Ready to use' - models

# Components of Electric Drives

- Sources
- Converters
- Electric machines
- Measurement devices
- Control units
- Mechanical loads

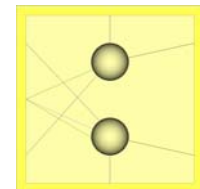
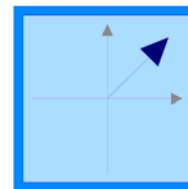
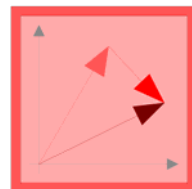
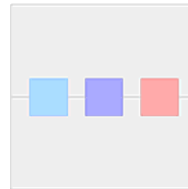


# 'Ready to use' Models

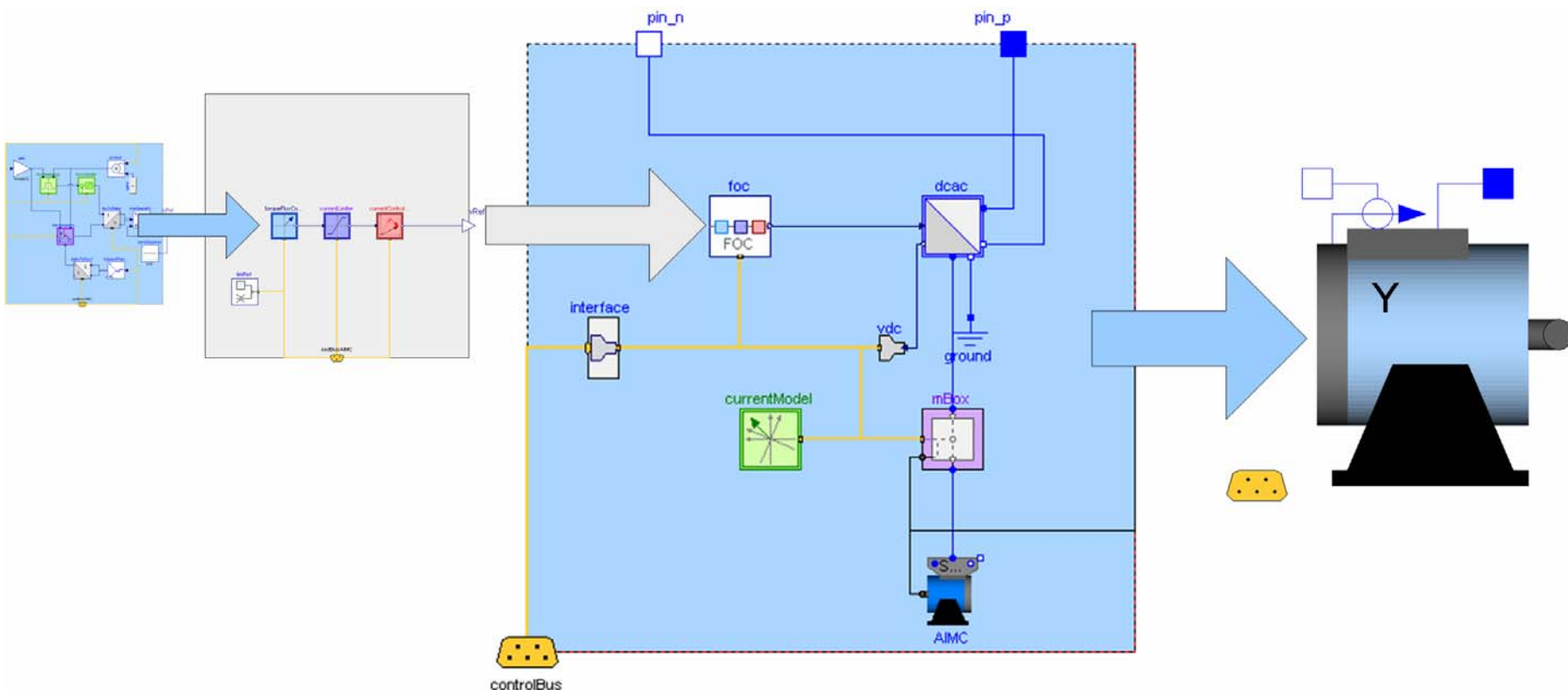


## ‘Ready to use’ Models

- Models of controlled machines
- Models of drive controllers
- Models of elementary controllers

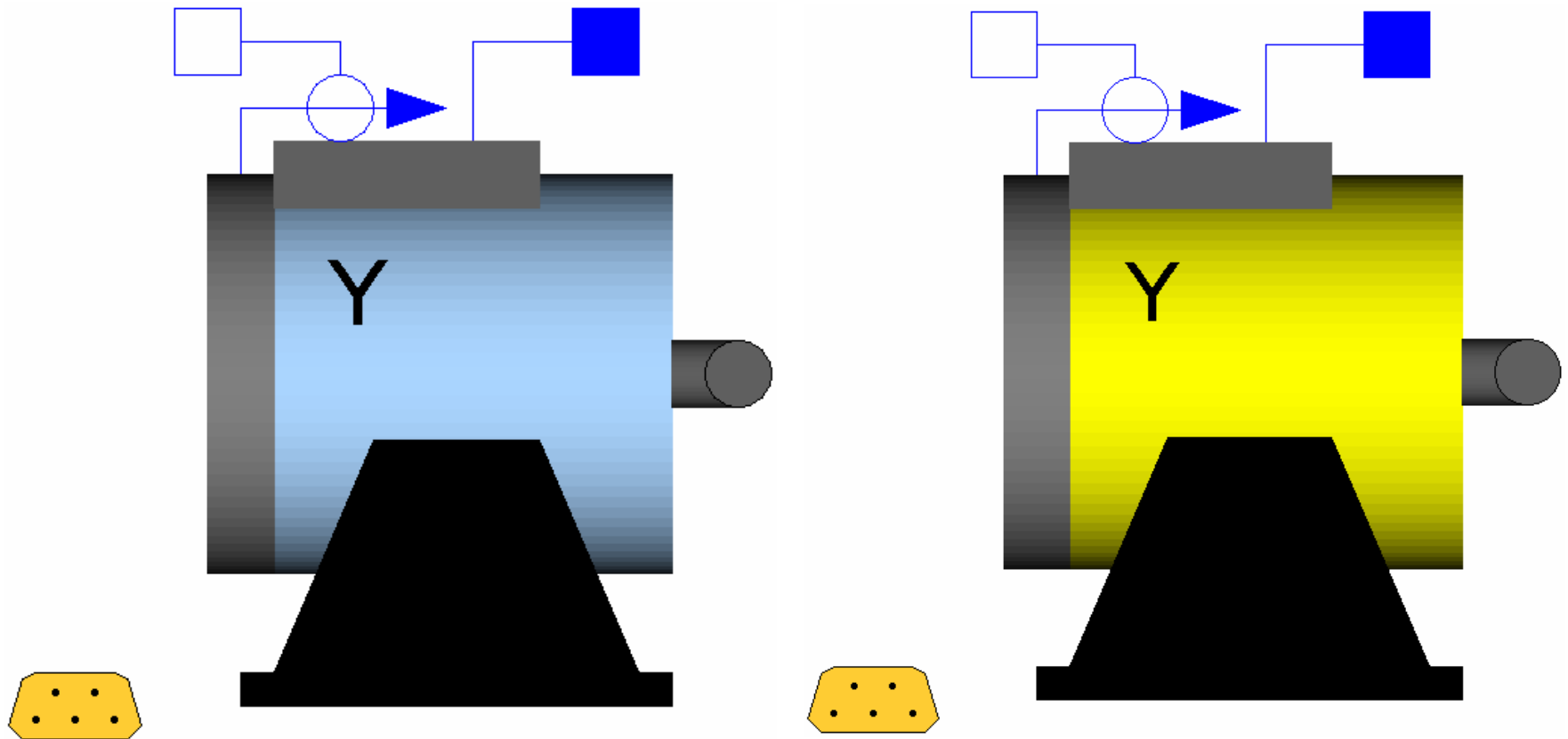


# Torque Controlled Induction Machine with Integrated Converter

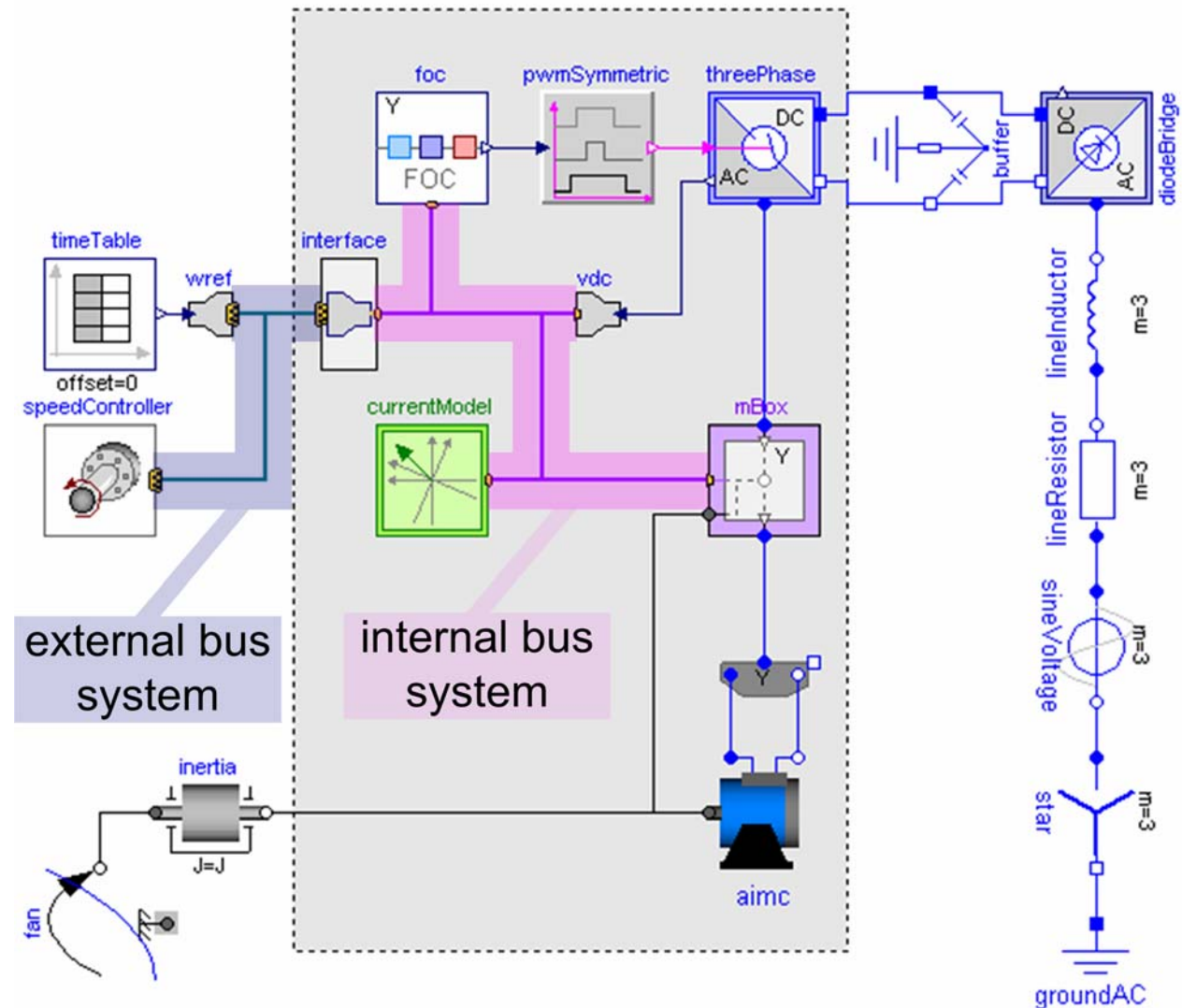









# Connectors of the Controlled Machine Models



# Bus concept

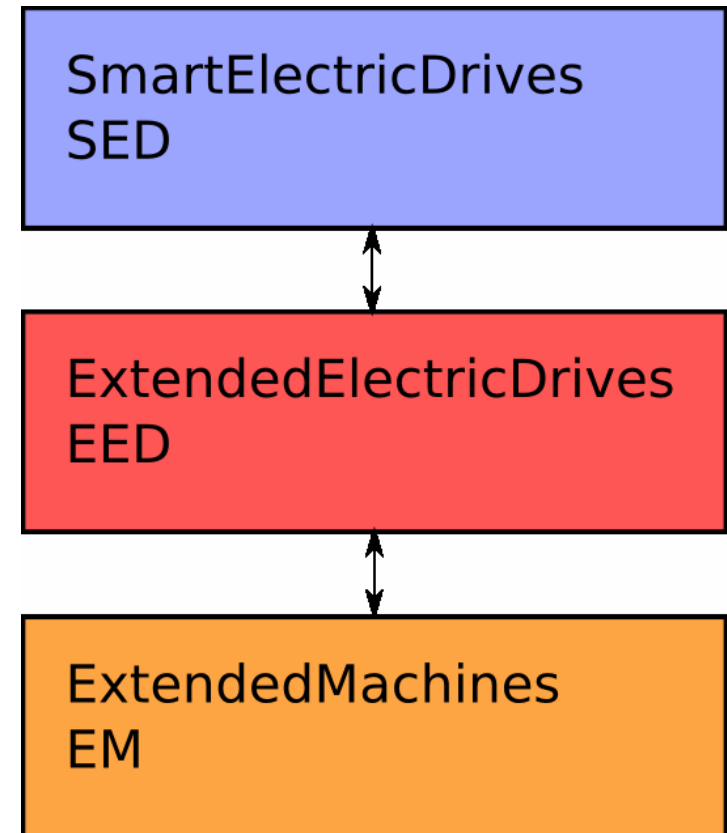


# Different levels of abstraction

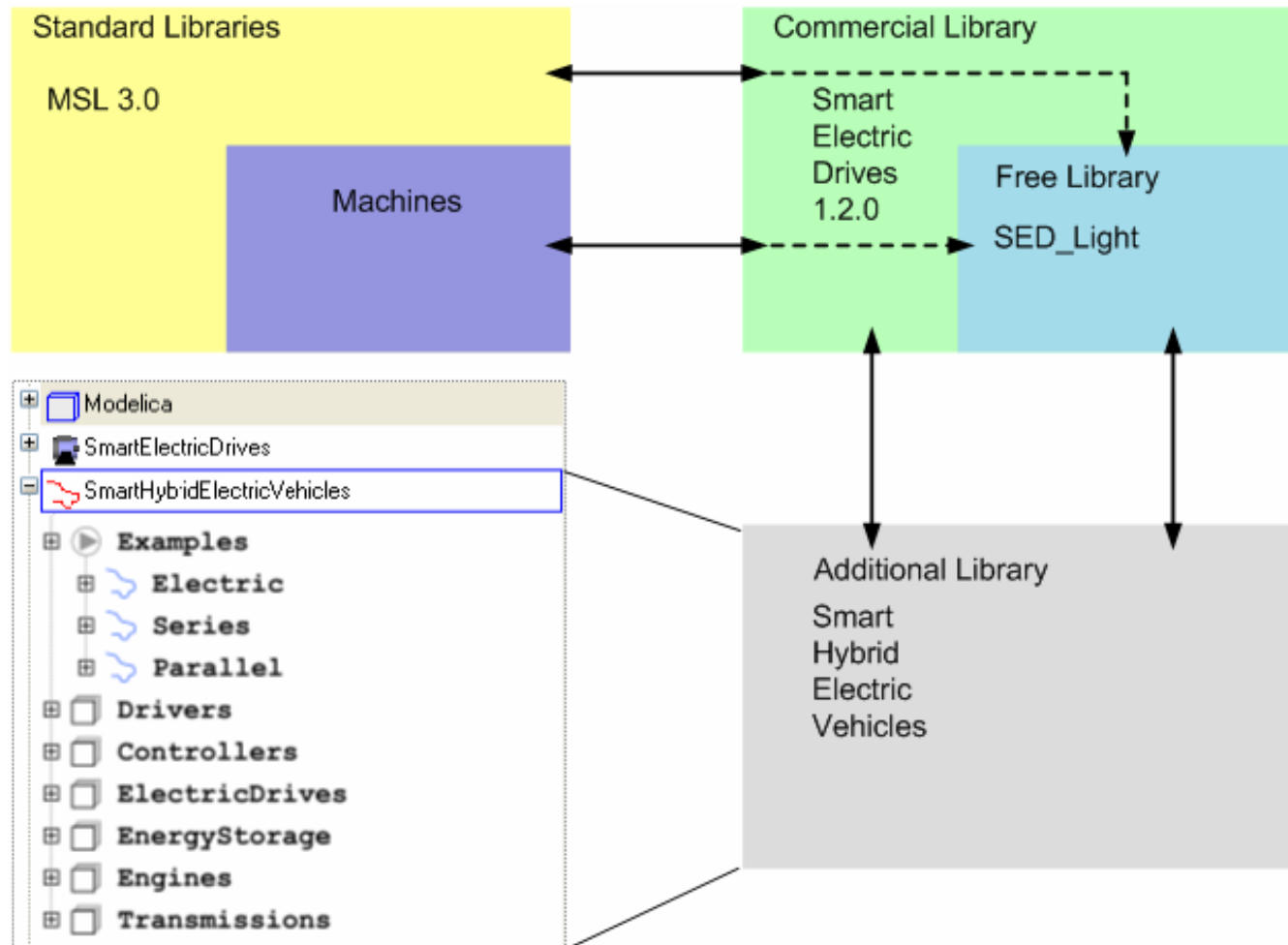
Models of controlled machines	Electrical transients and mechanical transients	
	Quasi stationary models (only mechanical transients)	
Converters	Power balance	
	Ideal switches	
	Real switches (coming soon)	

# Outlook

- Various number of phases of stator and rotor
- Asymmetric phase windings enable consideration of stator / rotor failures
- Saturation effects (induction / synchronous / dc machines)
- Deep bar effect of squirrel cage rotors (induction machines)
- Iron losses (hysteresis losses, eddy losses)
- Supplementary and friction losses
- Thermal models of induction machines



# Outlook

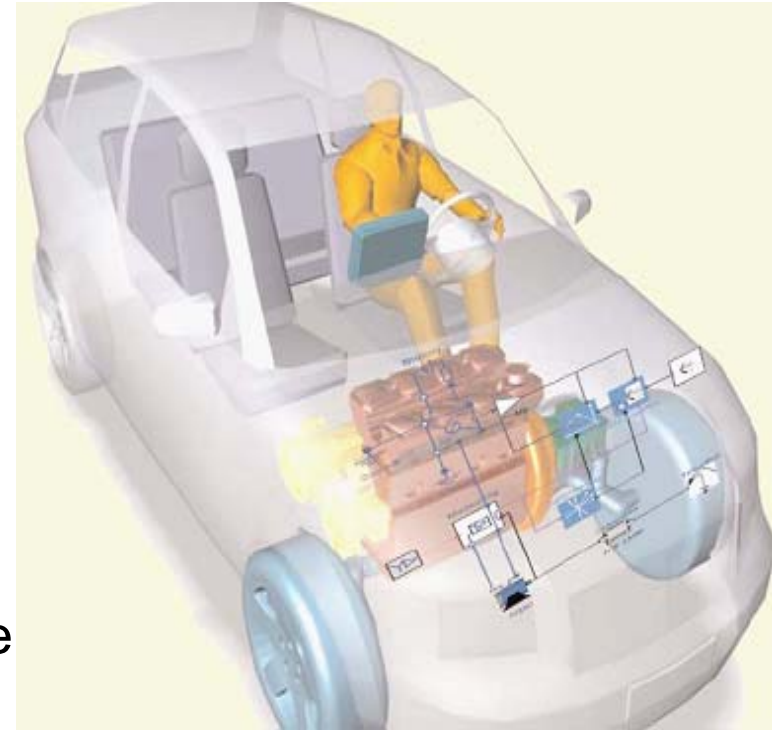


# Key Advantages of the SED library

- Comprehensive library for electric drive simulation in automotive applications
- Applicable for hardware in the loop (HIL) and real time simulations
- 'Ready to use' models
- Controller parameter estimation functions for easy controller handling
- Models at different layers of abstraction
- SED bus concept for easy coupling with other Dymola libraries
- Many examples, extensive documentation and intelligible SED library structure

## SED library – novelties

- SmartElectricDrives 1.2.0 – available now!
- Opened source code ~90 %
- SED light version for free – available since end of October!
- Additional HEV examples
  - SmartHybridElectricVehicles library coming soon (in combination with the SED library)



# Comparison SED library vs. SED light library

## SED library

- Sources
  - batteries, supercaps, fuel cells
- Converters
  - ideal, switching
- Electric machines
  - transient & quasi stationary models
  - asynchronous induction machines
  - permanent magnet synchronous induction machines
  - dc machines
- Control units
  - field oriented control, brushless dc control
- Electrical loads

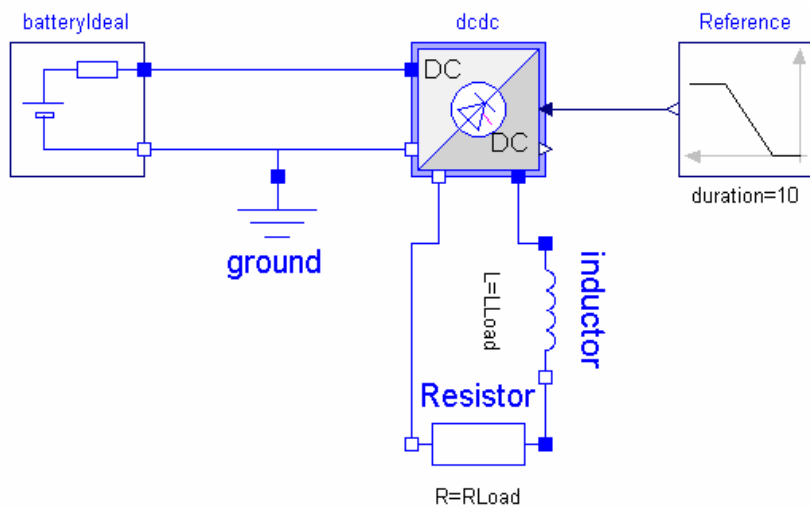
## SED light library version

- Sources
  - batteries
- Converters
  - restricted selection
- Electric machines
  - transient & quasi stationary models
  - dc machines
- Electrical loads
  - restricted selection



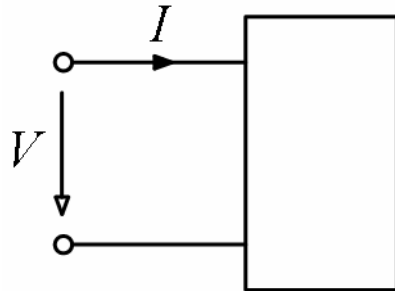
# DC Circuits

## Chapter 3



# Pulsating DC-Circuits

- Reason: power electronics with periodic behavior



$$p(t) = V \cdot I$$

$$P = \frac{1}{T} \int_0^T p(t) dt$$

- Characteristic quantities for periodic signals

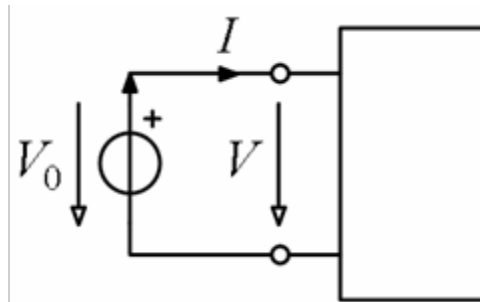
- Average values:

$$\bar{V} = \frac{1}{T} \int_0^T V(t) dt$$

$$\bar{I} = \frac{1}{T} \int_0^T I(t) dt$$

# Pulsating DC-Circuits

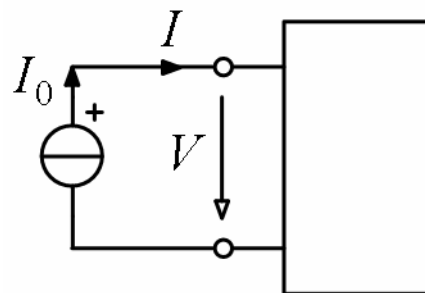
- Special cases
  - Constant voltage



$$P = V_0 \cdot \bar{I}$$

$$V = V_0$$

- Constant current

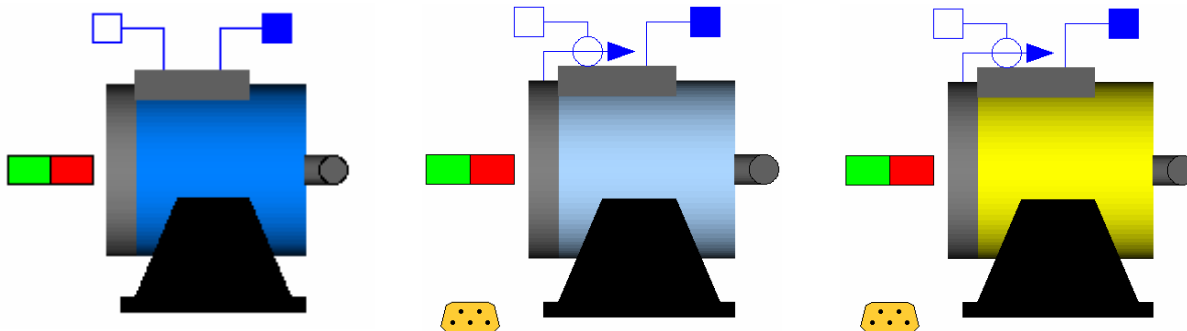


$$P = \bar{V} \cdot I_0$$

$$I = I_0$$

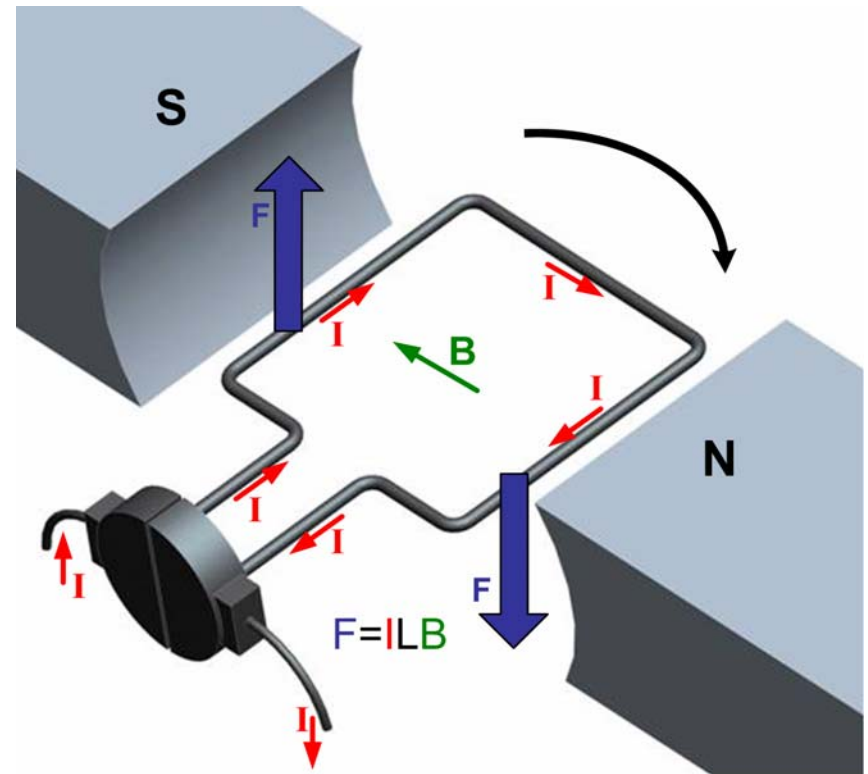
# DC Machines

## Chapter 4



# Principle

- The stator magnet creates a homogeneous magnetic field
- Opposite current direction in the proximity of the poles
- Same torque at all wires in the armature
- Commutator works as a mechanical rectifier



# The Equivalent Circuit

- Armature current  $I_a$

- Main flux  $\Phi$

- Induced voltage

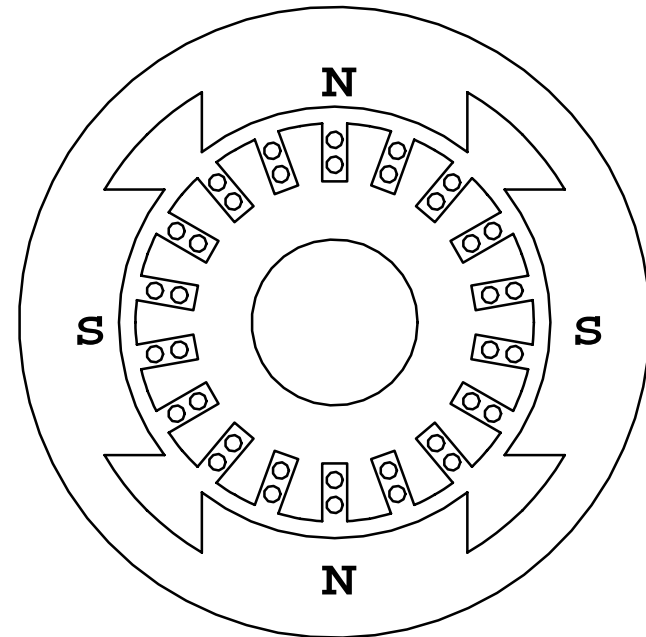
$$V_i = k \cdot \Phi \cdot \Omega_m$$

- Torque

$$T = k \cdot \Phi \cdot I_a$$

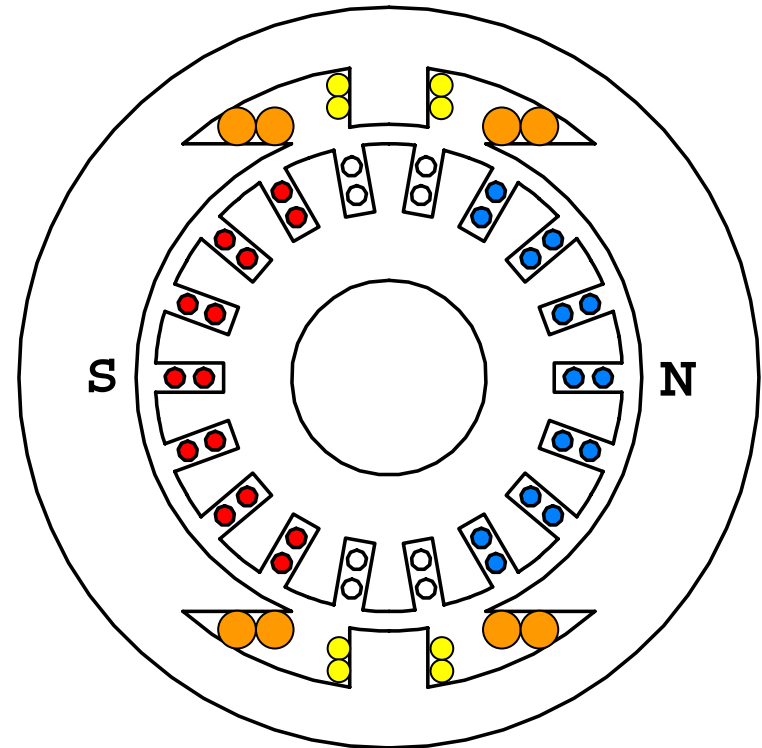
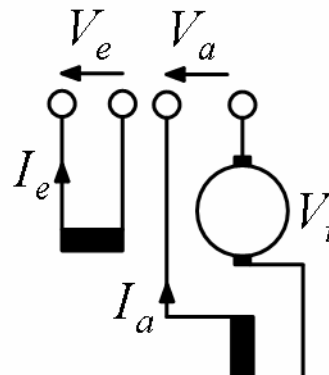
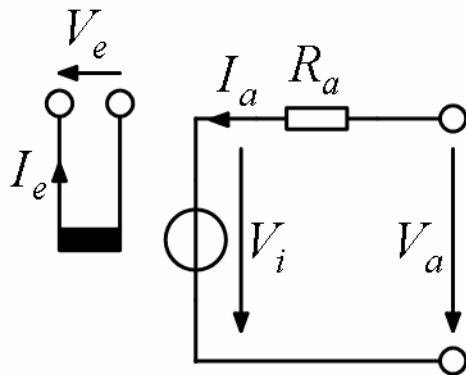
- Mechanical power

$$P_m = V_i \cdot I_a = T_{el} \cdot \Omega_m$$

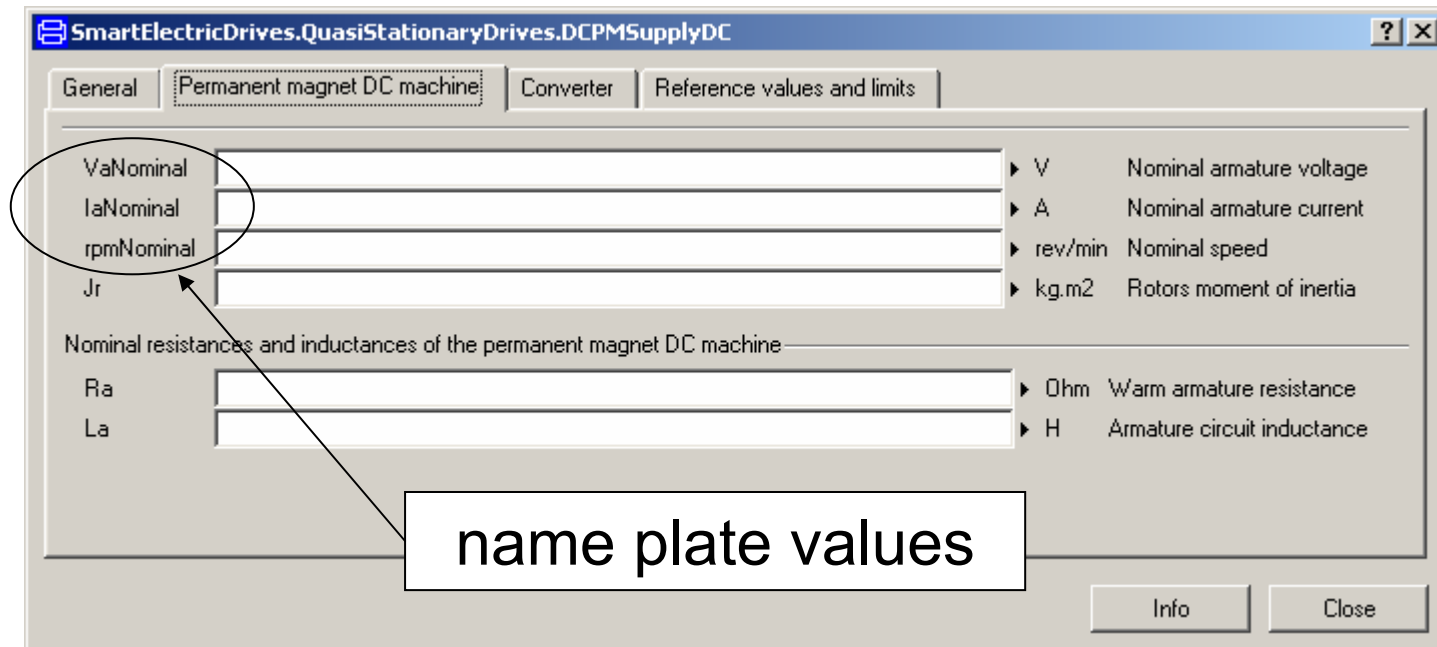


# The Equivalent Circuit – Steady State Operation

- Electrical excitation  $\Phi \propto I_e$   $V_i \propto \Phi \cdot \Omega_m$
- Armature circuit
- Excitation circuit (excitation current)
- Commutating poles



# Parameter List of the DCPM – Machine Model



SmartElectricDrives.QuasiStationaryDrives.DCPMSupplyDC

General | **Permanent magnet DC machine** | Converter | Reference values and limits

VaNominal		▶ V	Nominal armature voltage
IaNominal		▶ A	Nominal armature current
rpmNominal		▶ rev/min	Nominal speed
Jr		▶ kg.m <sup>2</sup>	Rotors moment of inertia

Nominal resistances and inductances of the permanent magnet DC machine

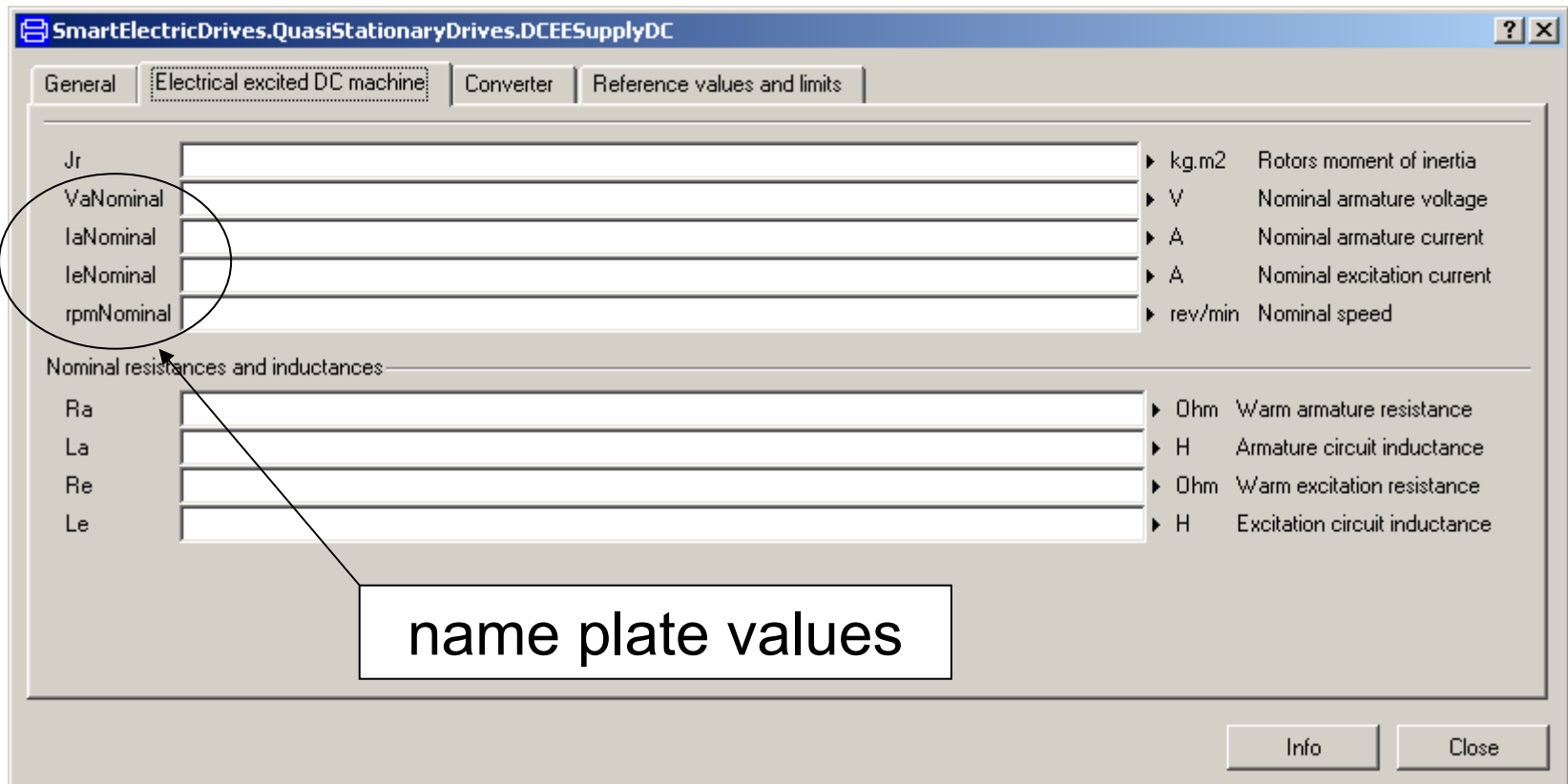
Ra		▶ Ohm	Warm armature resistance
La		▶ H	Armature circuit inductance

name plate values

Info Close



# Parameter List of the DCEE – Machine Model



SmartElectricDrives.QuasiStationaryDrives.DCEESupplyDC

General | **Electrical excited DC machine** | Converter | Reference values and limits

Jr		kg.m2	Rotors moment of inertia
VaNominal		V	Nominal armature voltage
IaNominal		A	Nominal armature current
IeNominal		A	Nominal excitation current
rpmNominal		rev/min	Nominal speed

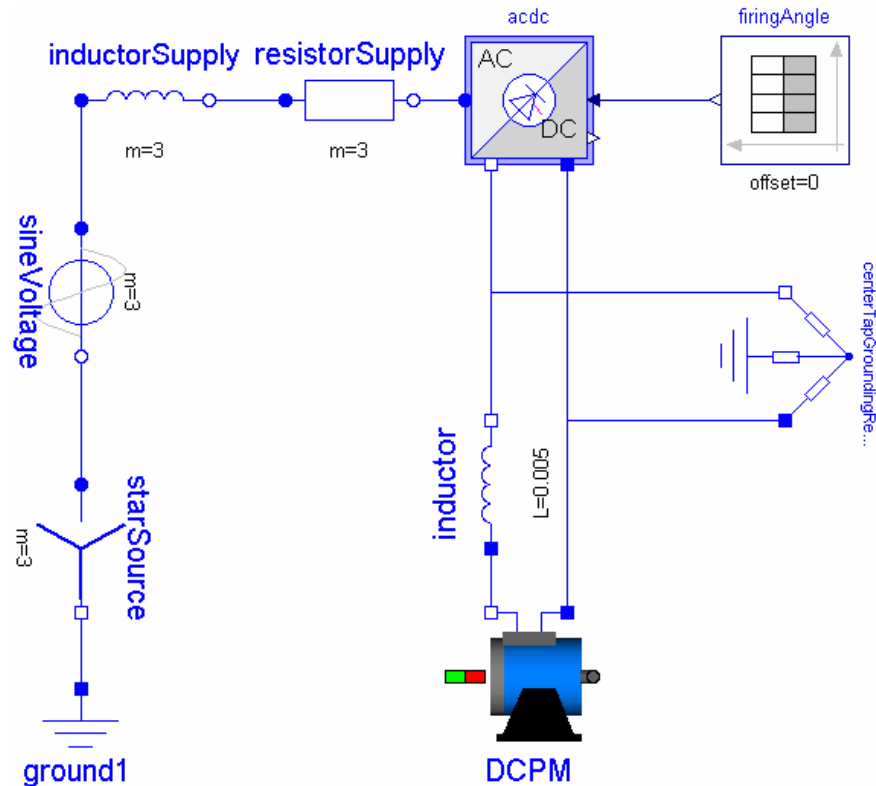
Nominal resistances and inductances

Ra		Ohm	Warm armature resistance
La		H	Armature circuit inductance
Re		Ohm	Warm excitation resistance
Le		H	Excitation circuit inductance

name plate values

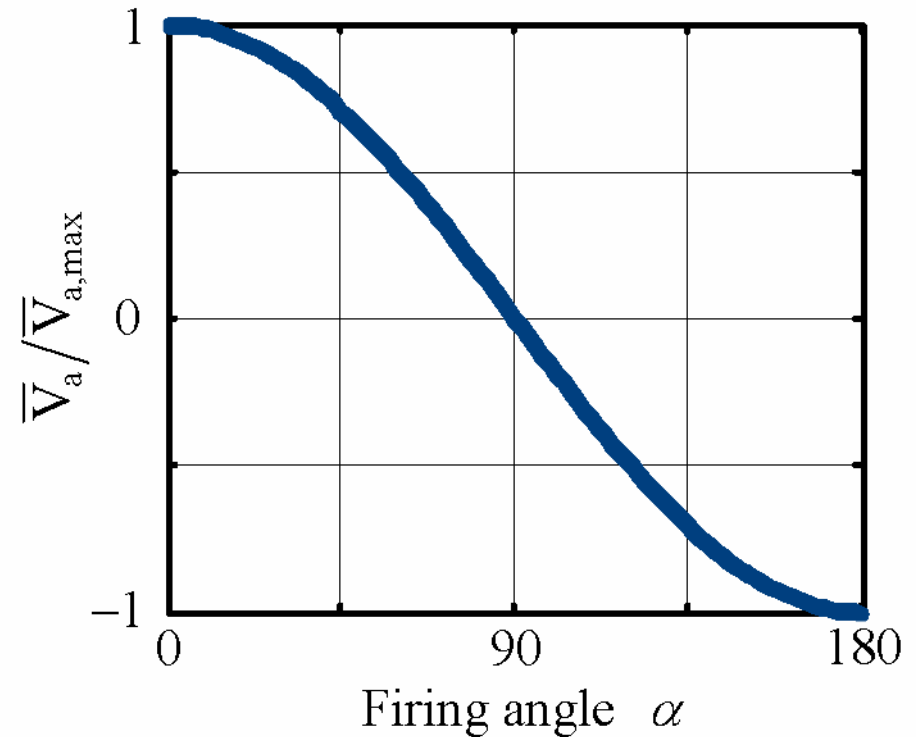
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# Three Phase Thyristor Bridge



# Three Phase Thyristor Bridge

- Voltage harmonics
- Current harmonics
  - Continuous mode
  - Discontinuous mode
- Through-conduction



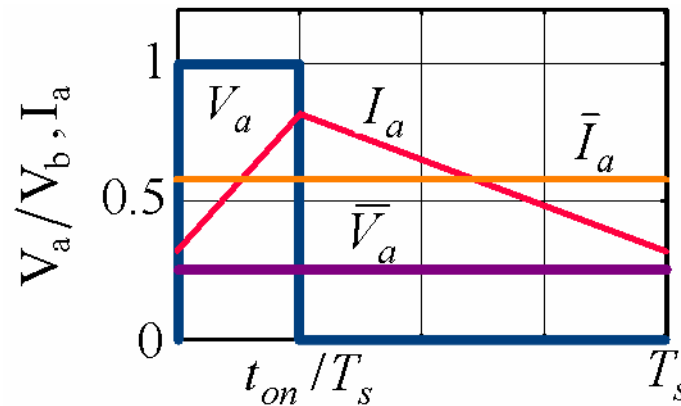
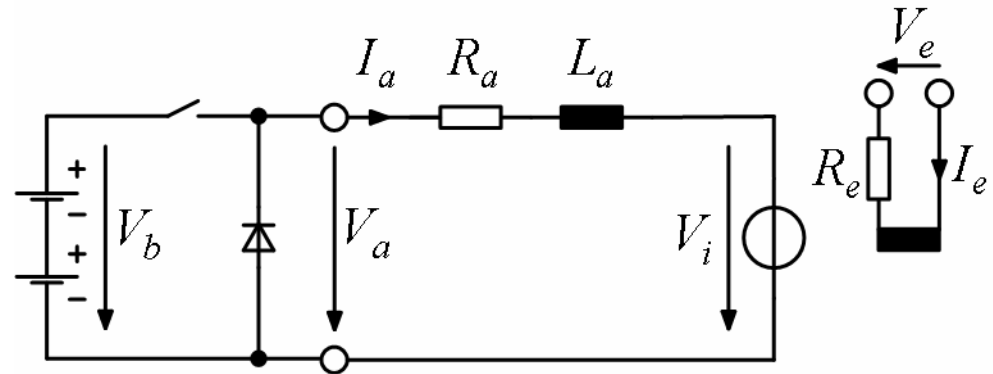
# Chopper

- DC supply
- Step down converter

$$- V_a = D \cdot V_s$$

$$- D = \frac{t_{on}}{T_s}$$

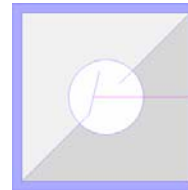
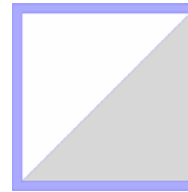
- Electric switches
- Free wheeling diode



$T_s$ :...switching periode

# Chopper Models in the SED Library

- Power balance model
  - low computing effort
- Ideal switching model
  - events
  - iteration
  - computing effort dependent on switching frequency



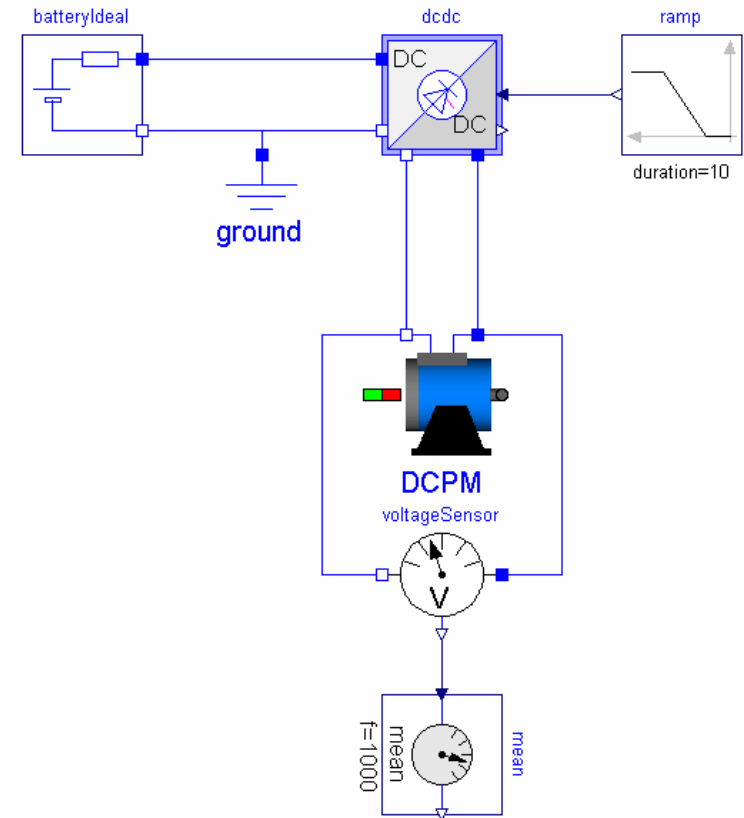
# Examples with a Chopper and a DC Machine

## Exercise 1

## SED Example – Chopper03

- Given:
  - Battery voltage = 100V
  - Reference voltage:  

$$\frac{dv}{dt} = \frac{100V}{10s} \quad V_{Max} = 100V$$
  - Chopper frequency = 1000Hz
- Display:  $i_a(t)$ ,  $v_a(t)$ ,  $\bar{I}_a$ ,  $\bar{V}_a$ ,  $\omega_m(t)$ 
  - Add an inertia
  - Add a load step



## Chopper03: Component Paths

- SmartElectricDrives.Sources.Batteries.BatteryIdeal
- Modelica.Electrical.Analog.Basic.Ground
- SmartElectricDrives.Converters.IdealSwitching.DCDC.Chopper
- Modelica.Blocks.Sources.Ramp
- Modelica.Electrical.Machines.BasicMachines.DCMachines. DC\_PermanentMagnet
- Modelica.Electrical.Analog.Sensors.VoltageSensor
- SmartElectricDrives.Sensors.Mean



## Chopper03: Parameter Settings

- BatteryIdeal
  - VCellNominal = 100V
  - ICellMax = 150A
  - RsCell = 0Ω
  - ns = 1
  - np = 1
- Chopper
  - f = 1000Hz
  - IConverterMax = 150A
  - VDC = 100V
- Ramp
  - height = 100
  - duration = 10s
- DCPM
  - Nominal values
- Mean
  - f = 1000Hz
  - yStart = 0
- Simulation time
  - t = 15s

## Chopper03: System Analyses

- Inertia added,  $J = 0.5 \text{kgm}^2$ 
  - **Compare:** batteryIdeal.IPackage, DCPM.w\_mechanical, DCPM.ia
  - The armature current increases
  - The shaft acceleration is delayed
  - The battery current drain increases
- Load added,  $T = -60 \text{Nm}$  @ 0.5s;  $J = 0 \text{kgm}^2$ ;
  - **Compare:** batteryIdeal.IPackage, DCPM.w\_mechanical, DCPM.ia

# SED Example – Chopper04

- Given:

- Battery voltage = 100V

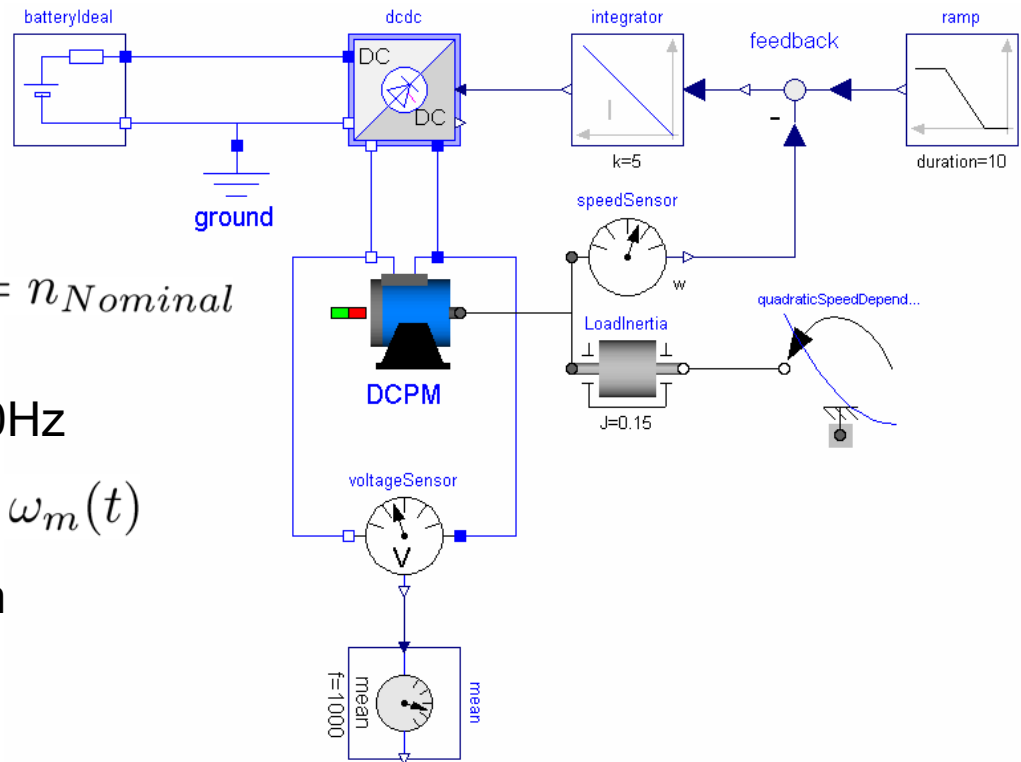
- Reference speed:

$$\frac{dn}{dt} = \frac{1425rpm}{10s} \quad n_{Max} = n_{Nominal}$$

- Chopper frequency = 1000Hz

- Display:  $i_a(t)$ ,  $v_a(t)$ ,  $\bar{I}_a$ ,  $\bar{V}_a$ ,  $\omega_m(t)$

- Change the integrator gain



## Chopper04: Component Paths

- SmartElectricDrives.Sources.Batteries.BatteryIdeal
- Modelica.Electrical.Analog.Basic.Ground
- SmartElectricDrives.Converters.IdealSwitching.DCDC.Chopper
- Modelica.Blocks.Continuous.Integrator
- Modelica.Blocks.Math.Feedback
- Modelica.Blocks.Sources.Ramp
- Modelica.Mechanics.Rotational.Sensors.SpeedSensor
- Modelica.Electrical.Machines.BasicMachines.DCMachines. DC\_PermanentMagnet
- Modelica.Mechanics.Rotational.Inertia
- Modelica.Mechanics.Rotational.QuadraticSpeedDependentTorque
- Modelica.Electrical.Analog.Sensors.VoltageSensor
- SmartElectricDrives.Sensors.Mean

# Chopper04: Parameter Settings

- BatteryIdeal
  - VCellNominal = 100V
  - ICellMax = 150A
  - RsCell = 0Ω
  - ns = 1
  - np = 1
- Chopper
  - f = 1000Hz
  - IConverterMax = 150A
  - VDC = 100V
- Integrator
  - k = 5
- Ramp
  - height = 149
  - duration = 10s
- DCPM
  - Nominal values
- Inertia
  - J = 0.15kgm<sup>2</sup>

# Chopper04: Parameter Settings

- QuadraticSpeedDependentTorque
  - $\tau_{\text{Nominal}} = -63.66 \text{ Nm}$
  - $\omega_{\text{Nominal}} = 149 \text{ rad}^{-1}$
- Mean
  - $f = 1000 \text{ Hz}$
  - $y_{\text{Start}} = 0$
- Simulation time
  - $t = 15 \text{ s}$

## Chopper04: System Analyses

- Integrator gain changed;  $k = 1$ , simulation time = 2s
  - **Compare:** DCPM.w\_mechanical, DCPM.ia, dcdc.vRef
  - The armature current decreases
  - The shaft acceleration is delayed
  - The reference voltage raise is delayed

## SED Example – Chopper05

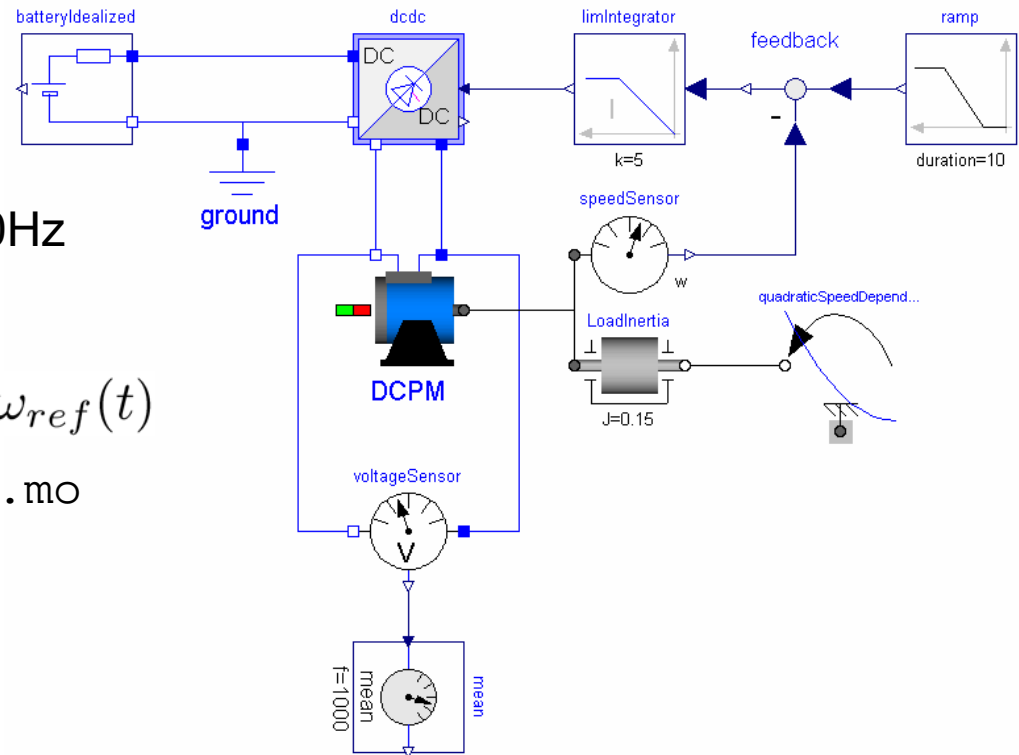
- Given:

- Reference speed : as in Chopper04
- Chopper frequency = 1000Hz

- Display:

$$i_a(t), v_a(t), \bar{I}_a, \bar{V}_a, \omega_m(t), \omega_{ref}(t)$$

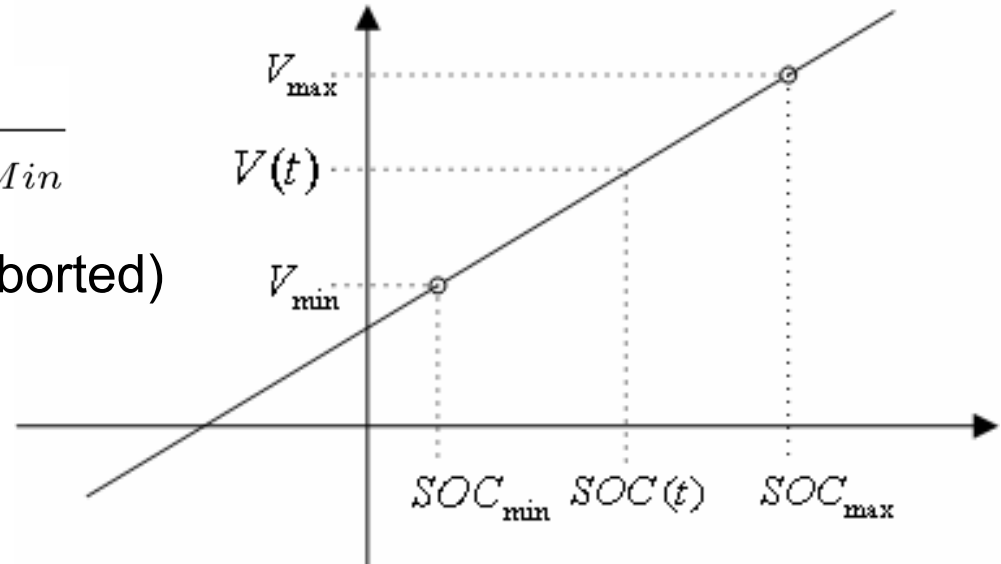
- Use batteryIdealized.mo
- Check SOC
- Add battery cells
- Change the controller limit





# Chopper05: Battery Model Parameterization

- Fictitious capacitance
  - $C = \frac{Q_{CellNominal}}{V_{CellMax} - V_{CellMin}}$
- Limits (simulation may be aborted)
  - $V_{CellMax}$
  - $I_{Max}$
- Total electric charge
  - $Q_{PackageNominal} = Q_{CellNominal} \cdot n_p$
- Total serial resistance
  - $R_{sPackage} = R_{sCell} \cdot \frac{n_s}{n_p}$



## Chopper05: Battery Model Parameterization

- Overall charging/discharging energy efficiency
  - heat losses due to the serial resistor (current dependent)
  - charge losses
- Overall charging/discharging efficiency always refers to a specific charging/discharging current  $I_{CellChargeDischarge}$ .
- Maximum possible efficiency of the battery without considering charge losses

$$efficiency_{Max} = \frac{(V_{CellMin} + V_{CellMax} - 2 \cdot R_{sCell} \cdot I_{CellChargeDischarge})}{(V_{CellMin} + V_{CellMax} + 2 \cdot R_{sCell} \cdot I_{CellChargeDischarge})}$$

## Chopper05: Component Paths

- SmartElectricDrives.Sources.Batteries.BatteryIdealized
- Modelica.Electrical.Analog.Basic.Ground
- SmartElectricDrives.Converters.IdealSwitching.DCDC.Chopper
- Modelica.Blocks.Continuous.LimIntegrator
- Modelica.Blocks.Math.Feedback
- Modelica.Blocks.Sources.Ramp
- Modelica.Mechanics.Rotational.Sensors.SpeedSensor
- Modelica.Electrical.Machines.BasicMachines.DCMachines. DC\_PermanentMagnet
- Modelica.Mechanics.Rotational.Inertia
- Modelica.Mechanics.Rotational.QuadraticSpeedDependentTorque
- Modelica.Electrical.Analog.Sensors.VoltageSensor
- SmartElectricDrives.Sensors.Mean

# Chopper05: Parameter Settings

- BatteryIdealized
  - QCellNominal = 36000C
  - VCellMin = 1V
  - VCellMax = 1.5V
  - SOCMin = 0.5
  - SOCMax = 0.8
  - SOCInit = 0.8
  - ICellMax = 100A
  - RsCell = 0.003Ω
  - Efficiency = 0.75
  - ICellChargeDischarge = 50A
  - ns = 66
  - np = 1
- Chopper
  - $f = 1000\text{Hz}$
  - IConverterMax = 150A
  - VDC = 100V
- Integrator
  - $k = 5$
  - outMax = 100
- Ramp
  - height = 149
  - duration = 10

## Chopper05: Parameter Settings

- DCPM
  - Nominal values
- Inertia
  - $J = 0.15 \text{ kgm}^2$
- QuadraticSpeedDependentTorque
  - $\text{TauNominal} = -63.66 \text{ Nm}$
  - $w\text{Nominal} = 149 \text{ rad}^{-1}$
- Mean
  - $f = 1000 \text{ Hz}$
  - $y\text{Start} = 0$
- Simulation time
  - $t = 15 \text{ s}$

## Chopper05: System Analyses

- The supply voltage decreases due to battery discharge
  - **Display:** dcdc.vRef, batteryIdealized.vPackage; ramp.y, DCPM.w\_mechanical; DCPM.ia; batteryIdealized.SOC;
  - To reach the desired speed the battery parameters must be changed.  $\rightarrow ns = 100$
- Controller limit changed; outMax = 1000
  - **Compare:** dcdc.vRef, batteryIdealized.vPackage; ramp.y, DCPM.w\_mechanical; DCPM.ia;
  - Without limiting the integrator the reference voltage would unnecessarily increase.

## SED Example – DCPMQS01

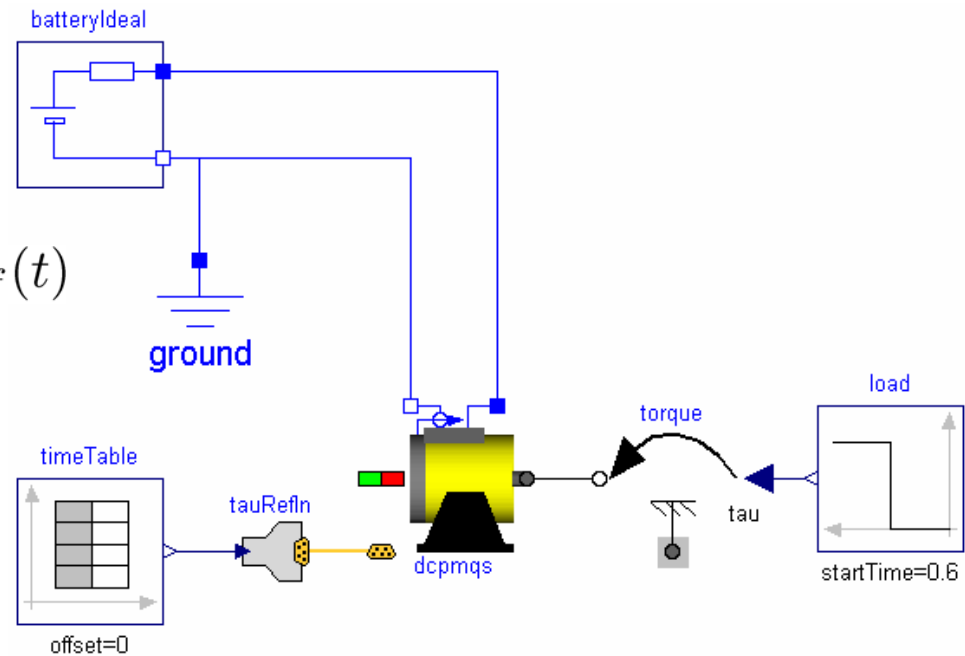
- Torque controlled DCPM

- Battery voltage = 120V

- Display:

$$i_a(t), v_a(t), \omega_m(t), \tau_{el}(t), \tau_{ref}(t)$$

- Check current limits
- Check voltage limits



## DCPMQS01: Component Paths

- SmartElectricDrives.Sources.Batteries.BatteryIdeal
- Modelica.Electrical.Analog.Basic.Ground
- Modelica.Blocks.Sources.TimeTable
- SmartElectricDrives.QuasiStationaryDrives.DCPMSupplyDC
- Modelica.Mechanics.Rotational.Torque
- Modelica.Blocks.Sources.Step



# DCCPMQS01: Parameter Settings

- BatteryIdeal
  - VCellNominal = 1.5V
  - ICellMax = 400A
  - RsCell = 0.004Ω
  - ns = 80
  - np = 2
- DCCPMQS
  - Jr = 0.15
  - VaNominal = 100V
  - IaNominal = 100A
  - rpmNominal = 1425rpm
  - (wNominal = 149s<sup>-1</sup>)
  - (TauNominal = 63.66Nm)
  - Ra = 0.05Ω
  - La = 0.0015Ω
  - TiConverter = 0.001s
  - vMachineMax = 1.1\*VaNominal
  - iMachineMax = 1.5\*IaNominal
  - IConverterMax = 2.5\*IaNominal

# DCPMQS01: Parameter Settings

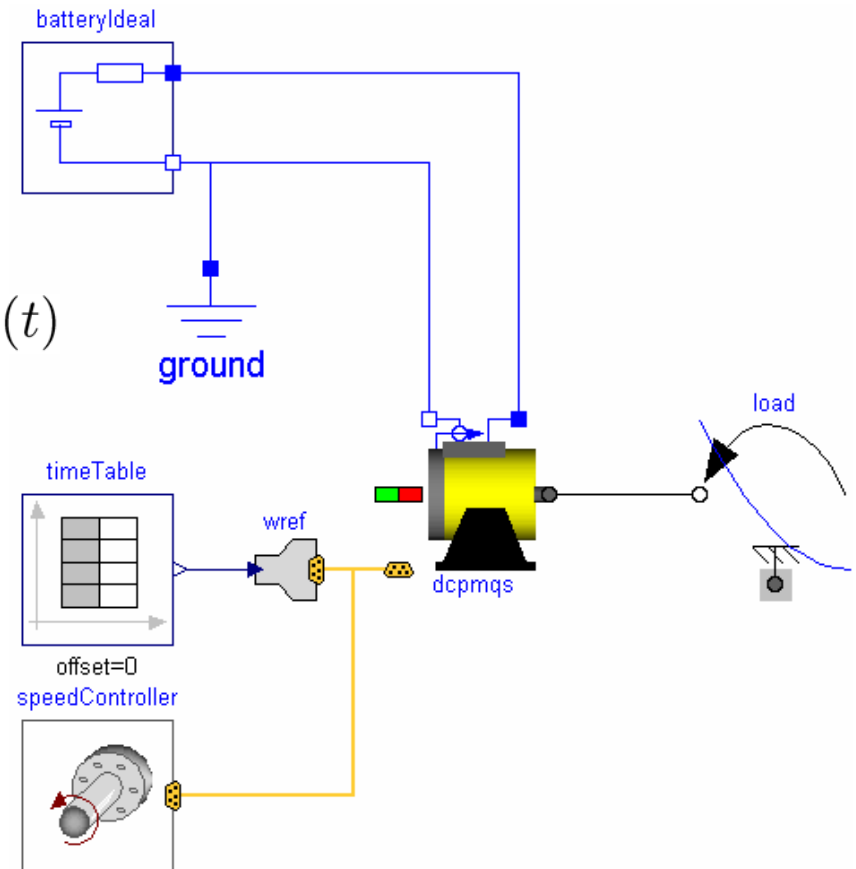
- TimeTable
  - [0, 0; 0.2, 0; 0.2, TauNominal/2; 0.4, TauNominal/2; 0.8, TauNominal/2; 0.8, TauNominal; 1, TauNominal]
  - Optional: [y = y(redeclare type SignalType = Modelica.SIunits.Torque)]
- Step (load)
  - height = -TauNominal/2
  - startTime = 0.6s
  - Optional: [add modifier: y(redeclare type SignalType = Modelica.SIunits.Torque)]
- Simulation time
  - t = 1s

## DCPMQS01: System Analyses

- The electric torque follows the reference torque instantly.
  - **Display from dcpmq.s.controlBus:** vMachine, vMachineMax, iMachine, iMachineMax, wMechanical, tauRef
  - **Display furthermore:** dcpmq.s.tauElectrical
- Current limit changed;  $I_{MachineMax} = 0.8 \cdot I_{aNominal}$ 
  - **Compare:** dcpmq.s.controlBus.iMachine, dcpmq.s.tauElectrical;
  - The electric torque gets limited.
- Voltage limit changed;  $V_{MachineMax} = 0.7 \cdot V_{aNominal}$ 
  - The electric torque settles to a value only opposing the load torque.

## SED Example – DCPMQS02

- DCPM Water pump drive
  - Battery voltage = 120V
  - Speed controlled
- Display:  $i_a(t)$ ,  $v_a(t)$ ,  $\omega_m(t)$ ,  $\omega_{ref}(t)$ 
  - Check current limits
  - Check voltage limits
  - Check Torque limit



## DCPMQS02: Component Paths

- SmartElectricDrives.Sources.Batteries.BatteryIdeal
- Modelica.Electrical.Analog.Basic.Ground
- Modelica.Blocks.Sources.TimeTable
- SmartElectricDrives.Interfaces.BusAdaptors.WRefIn
- SmartElectricDrives.QuasiStationaryDrives.DCPMSupplyDC
- Modelica.Mechanics.Rotational.QuadraticSpeedDependentTorque
- SmartElectricDrives.ProcessControllers.SpeedController
- SmartElectricDrives.AuxiliaryComponents.Functions.  
parameterEstimationDCPMControllers

## DCPMQS02: Parameter Settings

- BatteryIdeal
  - VCellNominal = 1.5V
  - ICellMax = 400A
  - RsCell = 0.004Ω
  - ns = 80
  - np = 2
- DCPMQS
  - Jr = 0.15
  - VaNominal = 100V
  - IaNominal = 100A
  - rpmNominal = 1425rpm
  - (wNominal = 149s<sup>-1</sup>)
  - (TauNominal = 63.66Nm)
  - Ra = 0.05Ω
  - La = 0.0015Ω
  - TiConverter = 0.001s
  - vMachineMax = 1.1\*VaNominal
  - iMachineMax = 1.5\*IaNominal
  - IConverterMax = 2.5\*IaNominal

## DCPMQS02: Parameter Settings

- TimeTable
  - table=[0, 0; 0, 0; 0.2, wNominal/2; 1, wNominal/2; 1.2, wNominal; 2, wNominal]
- QuadraticSpeedDependentTorque
  - TauNominal = -63.66Nm
  - wNominal = 149 rad<sup>-1</sup>
- parameterEstimationDCPMControllers
  - kdynaCurrent = 5
  - kdynSpeed = 1
  - (Not available in SED light)
- Speed Controller
  - kpSpeed = 29.3
  - TiSpeed = 0.024s
  - TauMax = 1.2\* TauNominal = 76Nm
- Simulation time
  - t = 2s

Not available in SED light

## Using the Parameter Estimation Function

- parameterEstimationDCPMControllers

SmartElectricDrives.AuxiliaryComponents.Functions.parameterEstimationD... ? X

parameterEstimationDCPMControllers

Description  
Estimation of controller parameters for permanent magnet DC machines

Inputs

VaNominal	100	V	Nominal armature voltage of the DC machine
IaNominal	100	A	Nominal armature current
rpmNominal	1425	rev/min	Rotor nominal speed
J	0.15	kg.m2	Total inertia of the machine and the mechanical load
Ra	0.05	Ohm	Warm armature resistance
La	0.0015	H	Armature inductance
kdynaCurrent	5		Dynamic gain of the current controller
kdynSpeed	1		Dynamic gain of the speed controller

OK Info Copy Call Execute Close

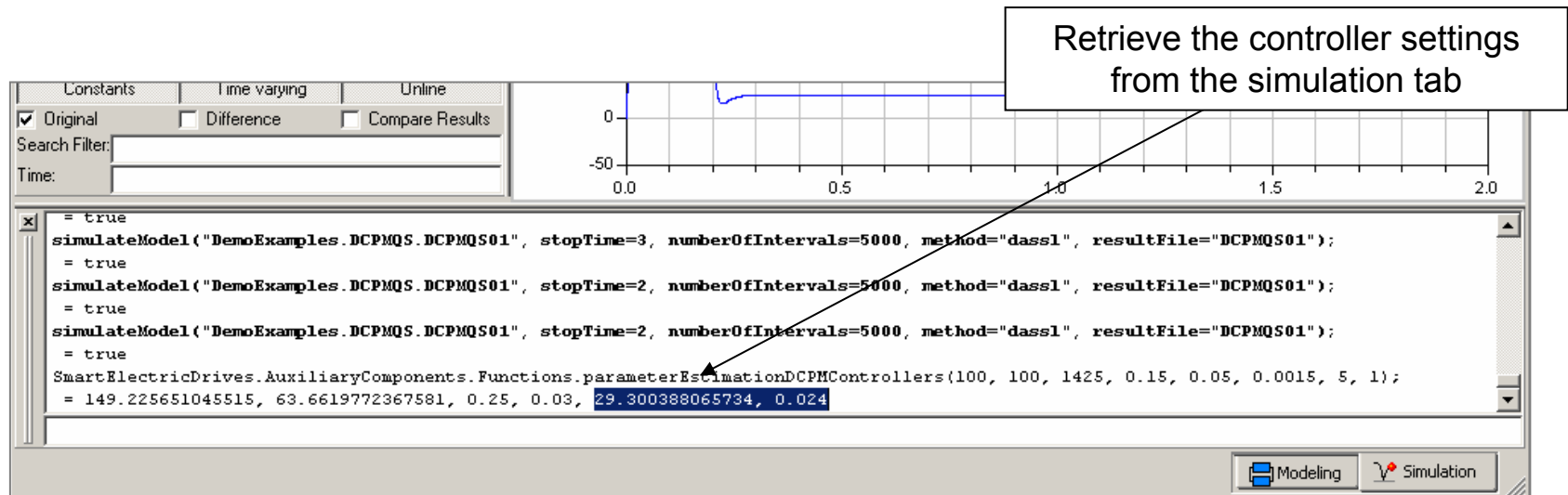
Generate controller settings



Not available in SED light

## Using the Parameter Estimation Function

- parameterEstimationDCPMControllers(VaNominal, IaNominal, rpmNominal, J, Ra, La, kdynaCurrent, kdynSpeed) = wNominal, TauNominal, kpaCurrent, TiaCurrent, kpSpeed, TiSpeed



## DCPMQS02: System Analyses

- The machine does not reach the desired acceleration close to  $w_{\text{Nominal}}$ .
  - **Display from dcpmq.s.controlBus:** vMachine, vMachineMax, vDC, iMachine, iMachineMax, wMechanical, wRef, tauRef
  - **Display furthermore:** speedController.TauMax
  - The torque limit TauMax is too low.
  - Increase TauMax and IMachineMax

# Exercise

## Conversion of a conventional vehicle to a hybrid electric vehicle with a starter-generator

### Software requirements:

SmartElectricDrives

SmartHybridElectricVehicles

PowerTrain

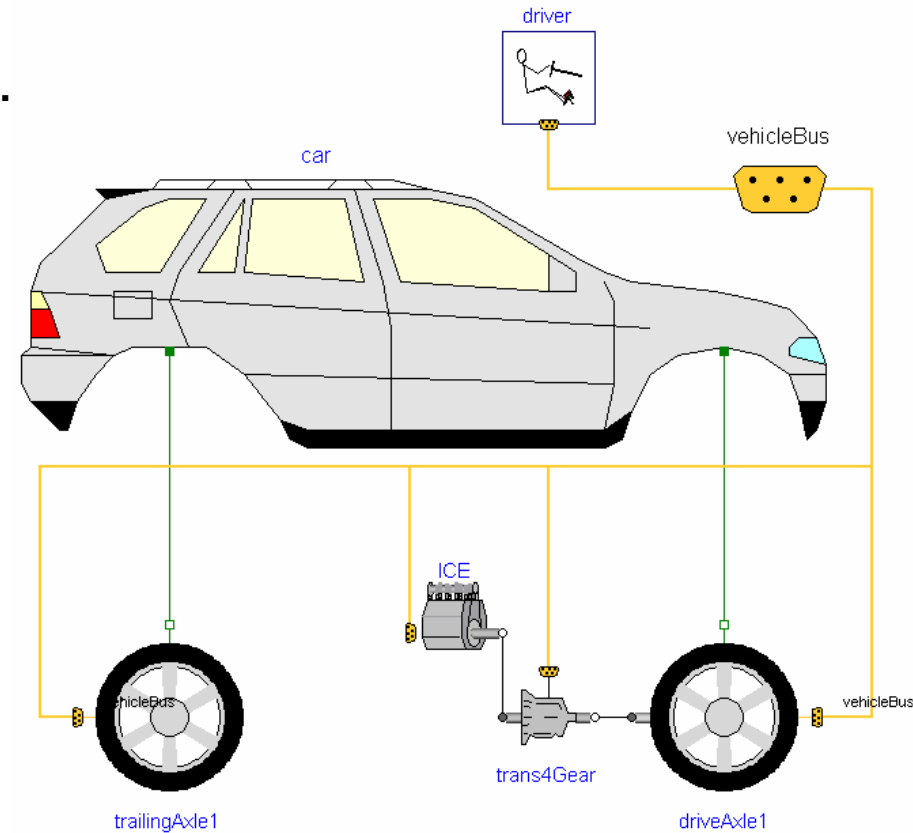
Dymola

## Work steps

- Take the conventional vehicle simulation
- Delete the unfit components
- Add the electrical components
- Add the automatic gearbox and the new controller
- Change the driver settings
- Connect the physical connectors
- Connect the signal bus connectors
- Run the simulation and assess the results

# Take the conventional vehicle simulation

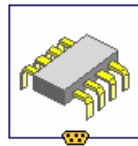
1. The conventional car model can be found in **SEDEXercise.Examples.ConventionalCars.ConventionalCar**.
2. Duplicate this model.
3. Call it **CarConversion1**.
4. Insert it in package **SEDEXercise.Work**.



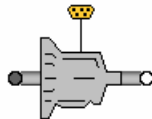
# Delete the unfit components

- Delete the components:

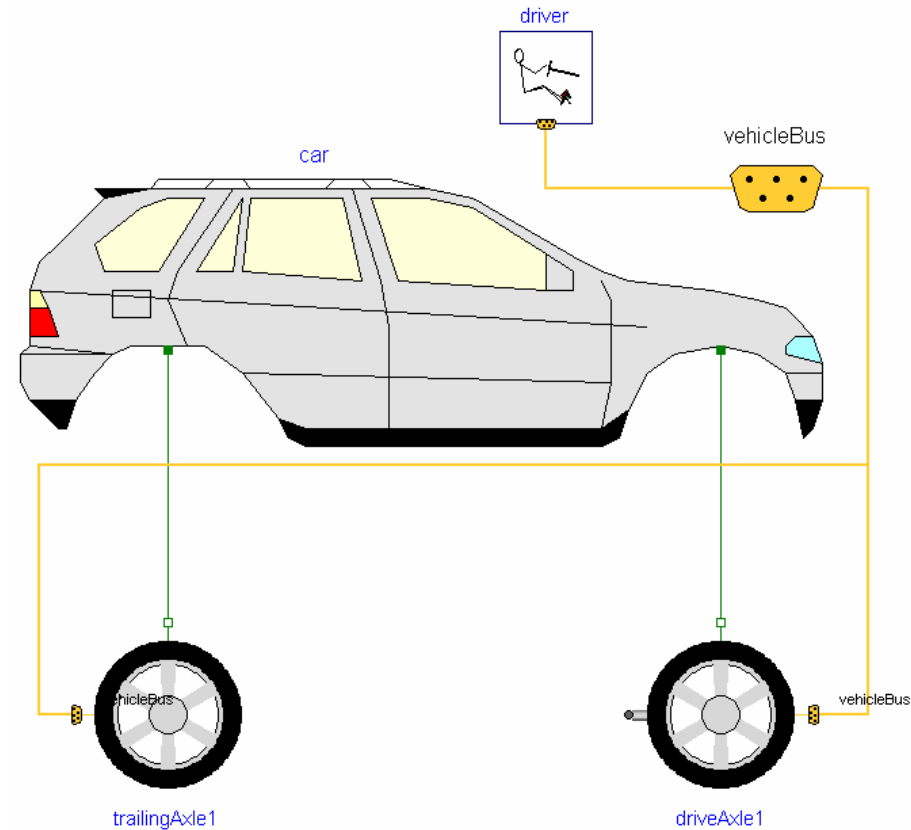
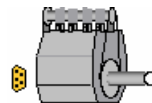
– **Controller**



– **Trans4gear**

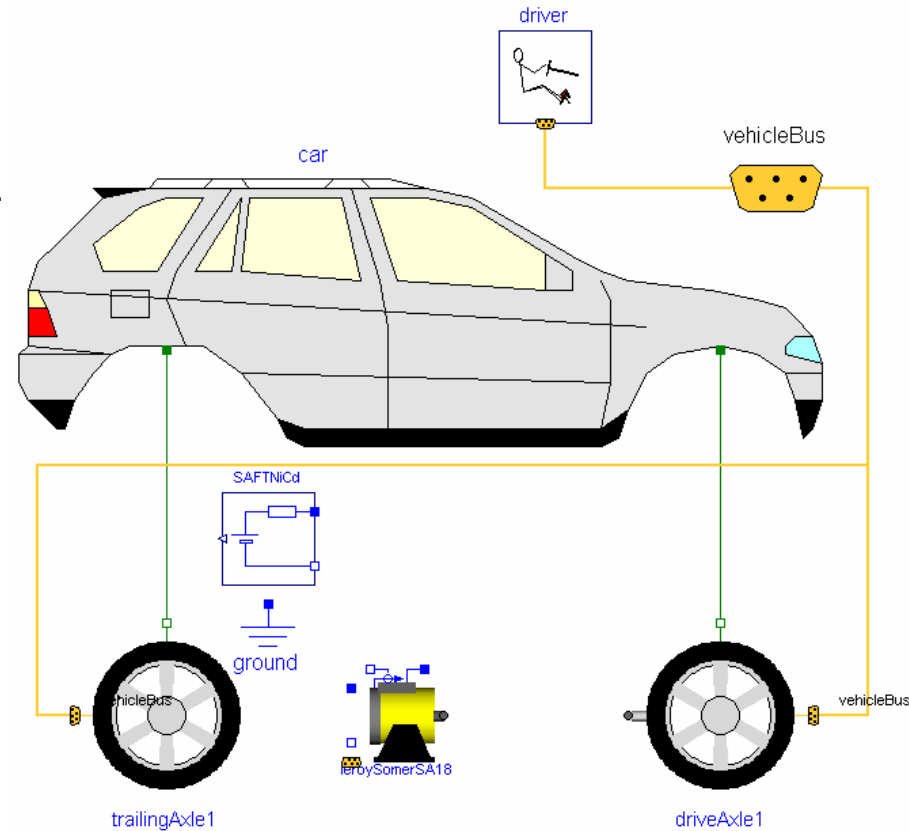


– **ICE**



# Add the electrical components

- Component paths:
  - `SmartElectricDrives.QuasiStationaryDrives.DCEESupplyDC`
  - `SmartElectricDrives.Sources.Batteries.BatteryIdealized`
  - `Modelica.Electrical.Analog.Basic.Ground`



# Parameters settings of the drive model

- DCEEQS
  - $V_{aNominal} = 162 \text{ V}$
  - $I_{aNominal} = 110 \text{ A}$
  - $I_{eNominal} = 9.5 \text{ A}$
  - $rpmNominal = 1650 \text{ rpm}$
  - $J_r = 0.2 \text{ kgm}^2$
  - $R_a = 0.23 \text{ } \Omega$
  - $L_a = 0.007 \text{ H}$
  - $R_e = 12.63 \text{ } \Omega$
  - $L_e = 1.263 \text{ H}$
- DCEEQS
  - $TiConverter = 0.001 \text{ s}$
  - $vMachineMax = 162 \text{ V}$
  - $iMachineMax = 220 \text{ A}$
  - $fluxLevel = 0.9$
  - $IConverterMax = 200 \text{ A}$
  - $ieMax = 19 \text{ A}$
  - $IeConverterMax = 19 \text{ A}$

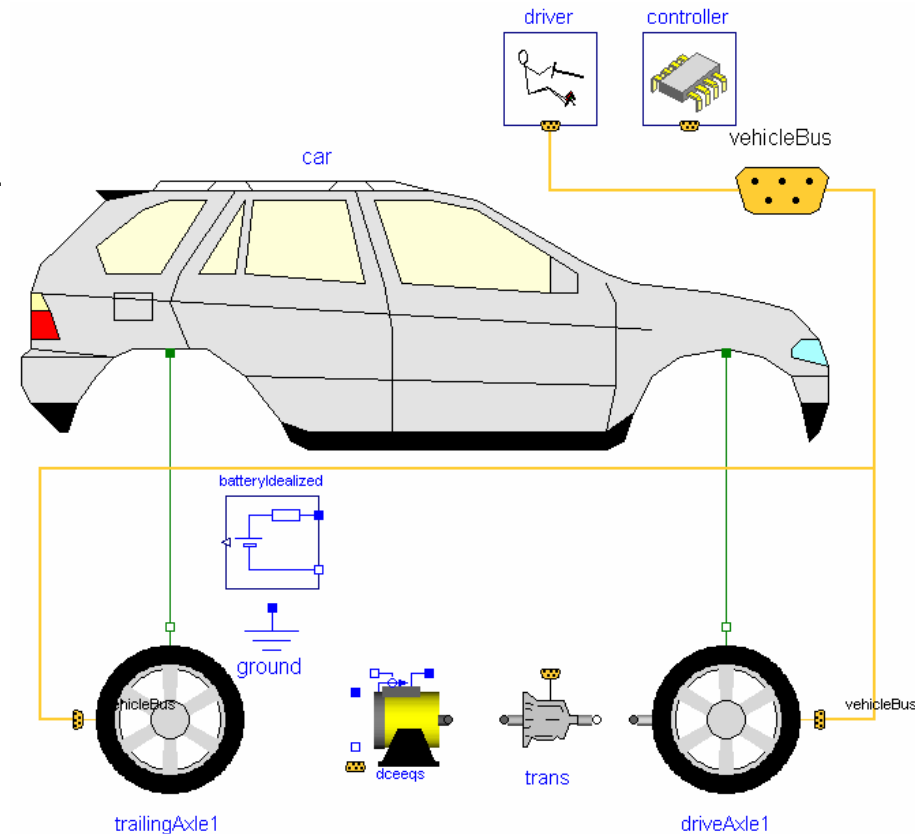


# Parameters settings of the battery model

- BatteryIdealized
  - QCell = 360000 C
  - VCellMin = 5.288 V
  - VCellMax = 6.315 V
  - SOCMin = 0
  - SOCMax = 1
  - SOCInit = 1
  - ICellMax = 150 A
  - RsCell = 0.0004  $\Omega$
  - efficiency = 0.8
  - ICellChargeDischarge = 100 A
  - ns = 27
  - np = 1

# Add the new gearbox and the new controller

- Component paths:
  - `SmartHybridElectricVehicles.VehicleTypes.ElectricCars.PeugeotPartnerLike.Controllers.TorqueControllerEDrive`
  - `SmartHybridElectricVehicles.VehicleTypes.ElectricCars.PeugeotPartnerLike.AuxiliaryComponents.CVTideal`

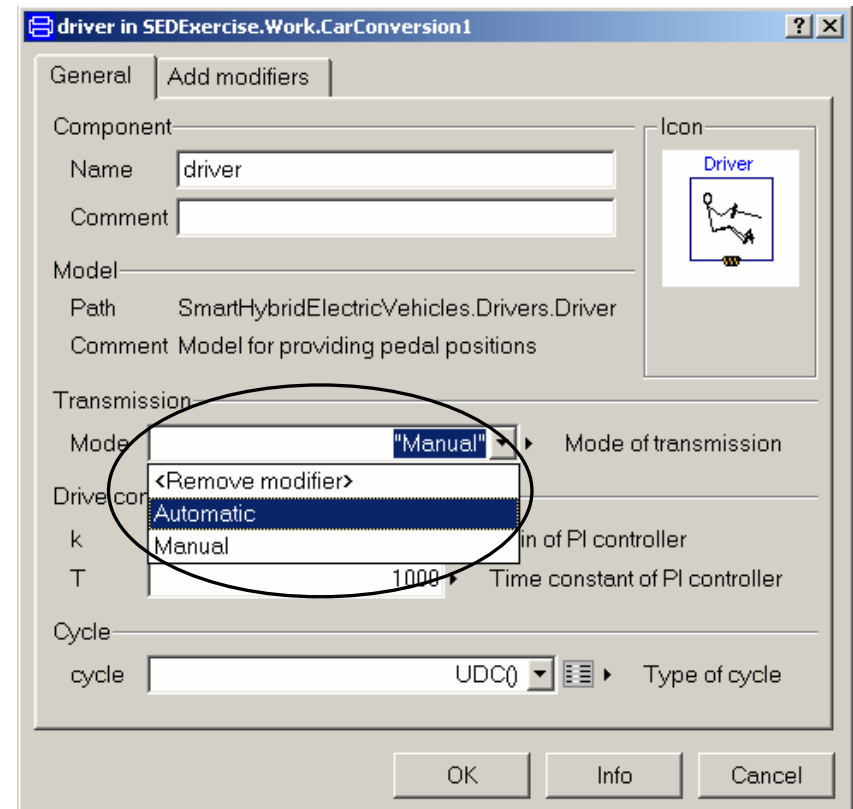


# Parameters settings of the gearbox model

- CVTideal
  - ratioMax = 2.88
  - ratioMin = 0.62
  - $J_{in} = 0.01 \text{ kgm}^2$
  - $J_{out} = 0.01 \text{ kgm}^2$

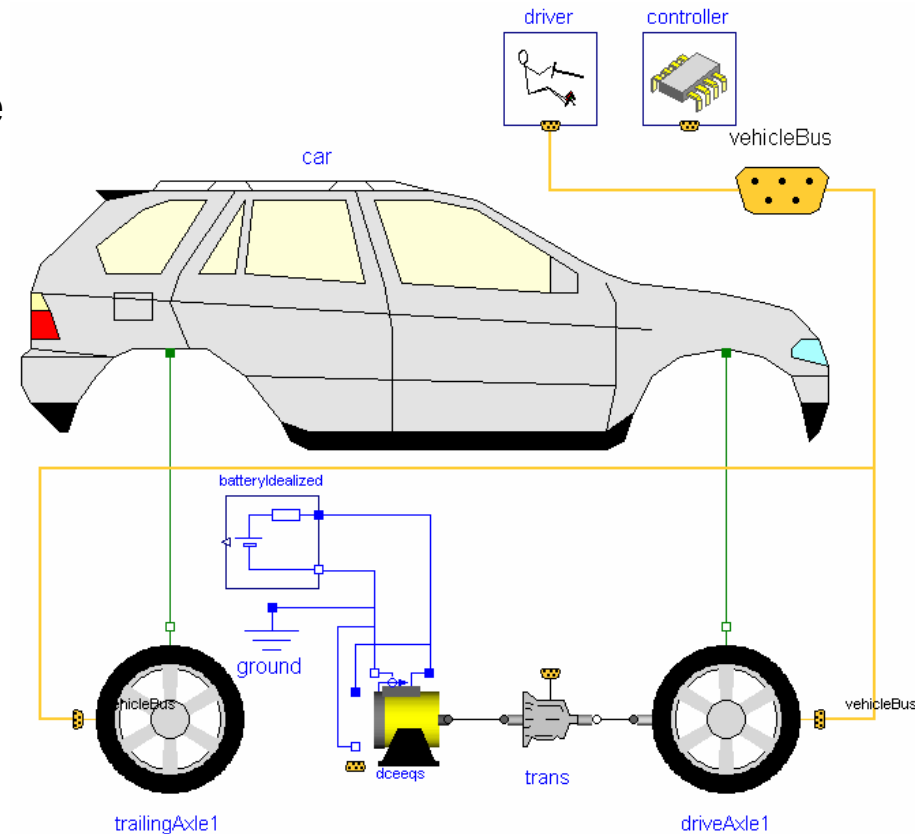
## Change the driver settings

- Since the old gearbox had to be operated manual and the new gearbox is automatic it is necessary to change the corresponding parameter setting to '**Automatic**' in the driver model.



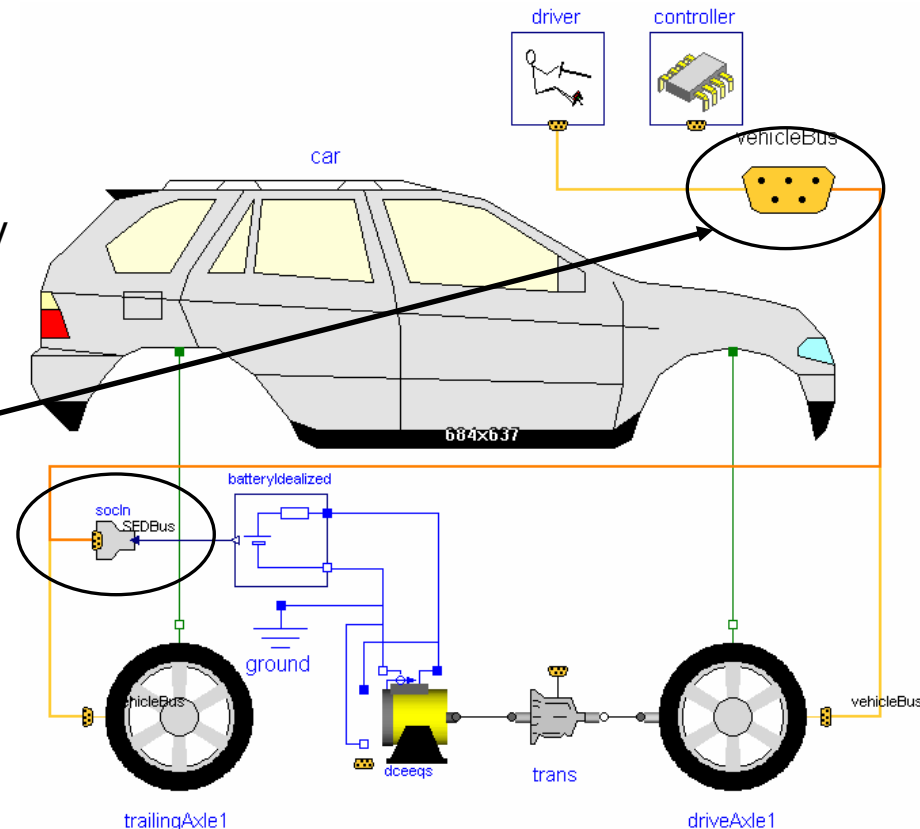
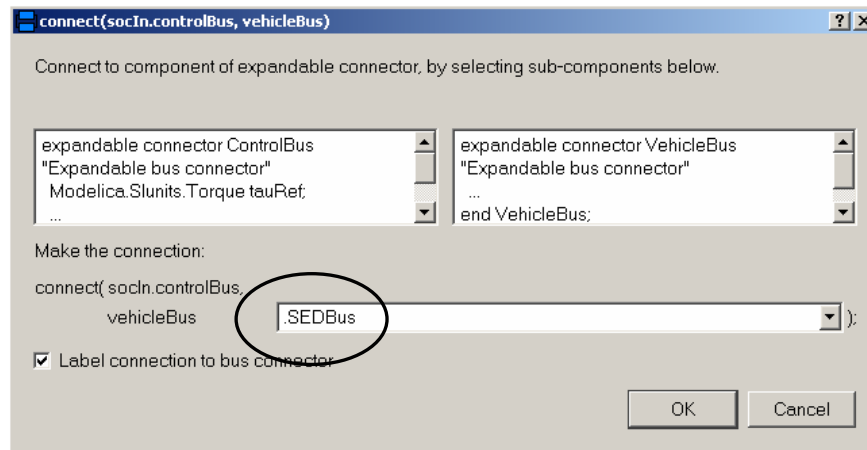
# Connect the physical connectors

- Note that the excitation circuit of the DC machine may be connected to the same DC link circuit as the armature circuit.
- The shaft of the DC machine may be connected via the gearbox to the front axle of the vehicle.



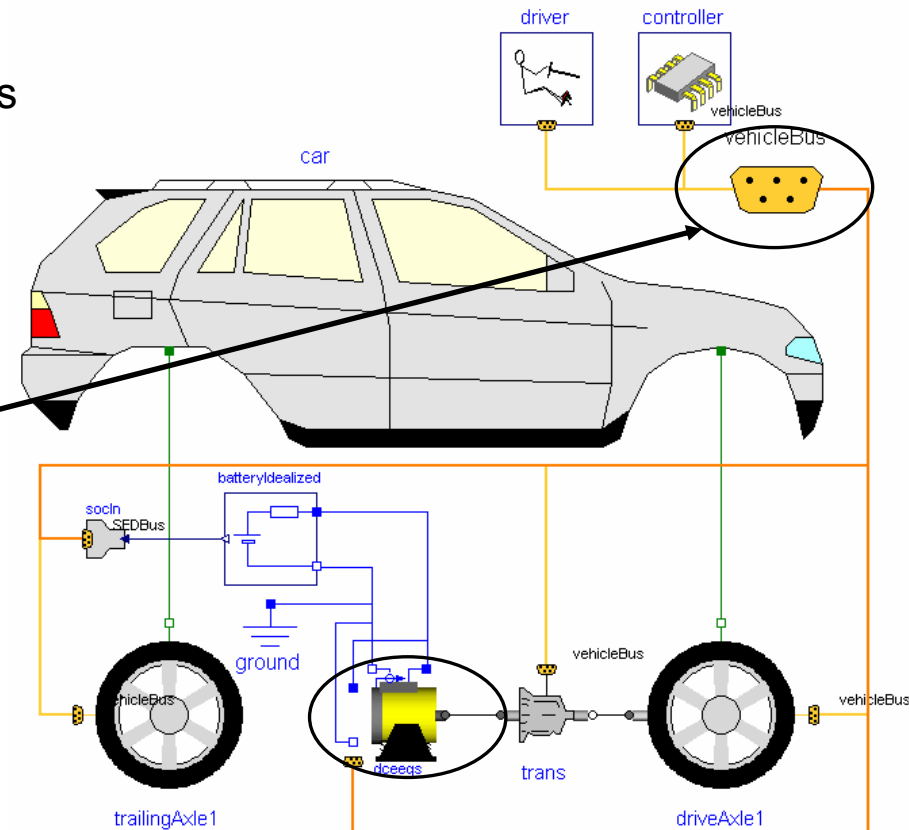
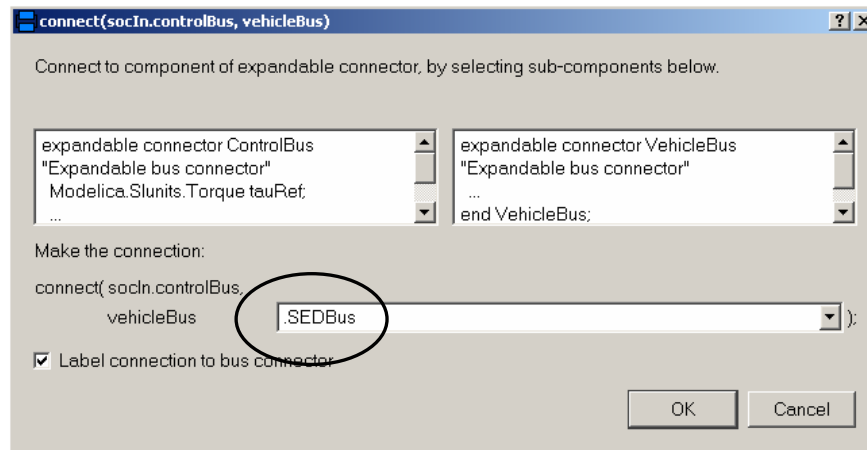
# Connect the signal bus connectors (1)

- Take the model **SmartElectricDrives.Interfaces.BusAdaptors.SOCIn** and connect it to the battery model.
- Connect this model with the vehicleBus by indicating the embedded bus system '**SEDBus**'.



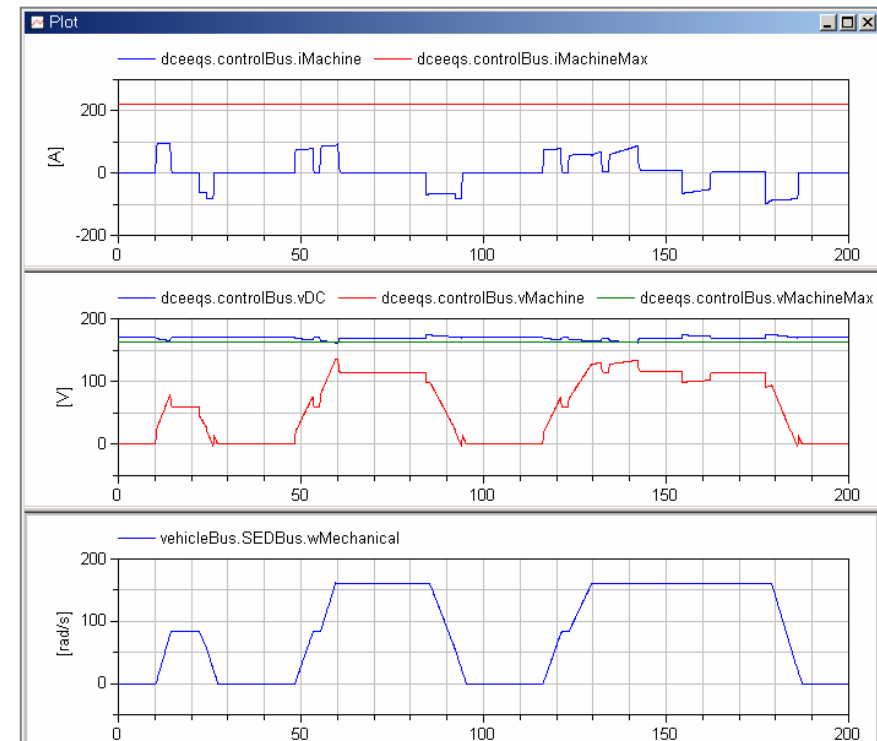
## Connect the signal bus connectors (2)

- Connect the drive model 'dceeqs' with the vehicleBus by indicating the embedded bus system '**SEDBus**'.
- Connect the controller model and the gearbox model with the vehicleBus on the top level (no specific indication).



# Run the simulation and assess the results

- Compare the urban drive cycle (UDC) and the full load drive cycle at 120km/h.
- The full load drive cycle at 150 km/h is not applicable for this model.
  - **Display:**  $v$ ,  $v_{Ref}$
  - **The most important machine parameters can be found in dceeqs.controlBus:**  $i_{Machine}$ ,  $i_{MachineMax}$ ,  $v_{Machine}$ ,  $v_{MachineMax}$ ,  $v_{DC}$ ,  $w_{Mechanical}$
  - **Display furthermore:** batteryIdealized.SOC





Thank you for the attention.

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# The SmartElectricDrives library

A powerful tool for electric drive simulation

